REPORT DOCUMENTATION PAGE

The examination of documents and visual inspection of the Site 1 Dam and appurtenant structures did not reveal conditions which constitute a hazard to

DD 1 FORM 1473 EDITION OF 1 NOV 65 IS OBSOLETE

human life or property.

SECURITY CLASSIFICATION OF

READ INSTRUCTIONS

BEFORE COMPLETING FORM

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The discharge capacity of the spillways is adequate for the PMF (Probable Maximum Flood).

The following remedial actions must be completed within 1 year from notification to the owner:

- 1. Eliminate the pedestrian and vehicular traffic on the embankment and the auxiliary spillway, backfill all depressions and reseed these areas.
- 2. Repair the erosion and reseed the areas adjacent to the impact basin, along the toe of the embankment, and between the right abutment and the auxiliary spillway outlet. Also remove the stockpiles in the channel and near the outlet of the auxiliary spillways and reseed.
- 3. Recaulk the joint between the service spillway pipe and the impact basin wall. Repair the concrete surfaces of the impact basin and the left animal guard.
- 4. Remove the vegetation along the left slope of the auxiliary spillway and on the banks of the downstream channel. Remove the debris on the approach channel of the auxiliary spillway. Provide a program of periodic cutting and mowing of the dam and appurtenances.
- 5. Provide a program of periodic inspection and maintenance of the dam and appurtenances, including yearly operation and lubrication of the reservoir drain system. Document this information for future reference. Also develop an emergency action plan.

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
PATTERSON, BRIXIUS, GREY CREEK
WATERSHED PROJECT - SITE 1
I.D. No. NY 698
DEC #86B-3457
SUSQUEHANNA RIVER BASIN
BROOME COUNTY, NEW YORK

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G.

DRAWINGS

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Patterson Brixius Grey Creek Watershed Project,

Site 1 I.D. No. NY 698

State Located:

New York

County Located:

Broome

Stream:

Patterson Creek (tributary of the

Susquehanna River)

Date of Inspection:

July 23, 1980

ASSESSMENT

The examination of documents and visual inspection of the Site 1 Dam and appurtenant structures did not reveal conditions which constitute a hazard to human life or property.

The discharge capacity of the spillways is adequate for the PMF (Probable Maximum Flood).

The following remedial actions must be completed within 1 year from notification to the owner:

- 1. Eliminate the pedestrian and vehicular traffic on the embankment and the auxiliary spillway, backfill all depressions and reseed these areas.
- 2. Repair the erosion and reseed the areas adjacent to the impact basin, along the toe of the embankment, and between the right abutment and the auxiliary spillway outlet. Also remove the stockpiles in the channel and near the outlet of the auxiliary spillways and reseed.
- 3. Recaulk the joint between the service spillway pipe and the impact basin wall. Repair the concrete surfaces of the impact basin and the left animal guard.
- 4. Remove the vegetation along the left slope of the auxiliary spillway and on the banks of the downstream channel. Remove the debris on the approach channel of the auxiliary spillway. Provide a program of periodic cutting and mowing of the dam and appurtenances.
- 5. Provide a program of periodic inspection and maintenance of the dam and appurtenances, including yearly operation and lubrication of the reservoir drain system. Document this information for future reference. Also develop an emergency action plan.

Dooge Boch

George Koch
Chief, Dam Safety Section
New York State Department of
Environmental Conservation
NY License No. 45937

Approved By:

Gol. W. M. Smith Jr. New York District Engineer

Date:

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Photo #1 Overview of Patterson Brixius Site 1 Dam

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PHASE I INSPECTION REPORT

NATIONAL DAM SAFETY PROGRAM
PATTERSON, BRIXIUS, GREY CREEK

WATERSHED PROJECT SITE 1 (Live: for Num 1.5 m NY698)

LB. No. MY 698

DEC 1065-3457

SUSQUEHANNA RIVER BASIN,

BROOME COUNTY, NEW YORK: Prace I I

10 George /Floch

SECTION 1: PROJECT INFORMATION

1.1 GENERAL

a. Authority
The Phase I Inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367.

b. Purpose of Inspection
Evaluation of the existing conditions of the subject dam to identify deficiencies and hazardous conditions, determine if they constitute hazards to life and property and recommend remedial measures where necessary.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances

The Site 1 Dam consists of a 1300 feet long homogeneous earth embankment with an auxiliary spillway located at the right end of the embankment in a cut section beyond the abutment of the embankment. The maximum height of the dam is 65 feet. The embankment has a crest width of 20 feet, an upstream slope of 1 vertical on 3 horizontal, and a downstream slope of 1 on 2.5. Two berms, located near the principal spillway riser on the upstream slope, were incorporated into the design.

>The auxiliary spillway is a vegetated earth channel, with a bottom width of 340 feet and side slopes of 1 on 3 (left slope) and 1 on 2 (right slope).

The principal spillway is a rectangular concrete riser which extends above the upstream slope near the toe of slope. The riser is topped by a triangular trash rack, the sides of which form a drop inlet, which is utilized during high reservoir levels. Under low flow conditions, a rectangular low stage inlet, in the upstream face of the riser, controls the reservoir level.

A 30 inch diameter reinforced concrete pipe controls the flow between the riser and the impact basin located at the toe of the dam. An 18 inch diameter pipe, with a manually operated slide gate, the controls of which are located atop the riser, serve as the reservoir drain system.

The dam is located on Patterson Creek, a tributary of the Susquehanna River, approximately 1 mile north of Endwell, New York.

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c. Size Classification

The dam is 65 feet high and is classified as "intermediate" in size (40 to 100 feet in height).

d. Hazard Classification

The dam is classified as high hazard because of its location above Endwell, New York.

e. Ownership

The dam is owned and operated by the County of Broome, New York.

f. Purpose

The dam is a floodwater retarding structure.

g. Design and Construction History

The dam was designed and construction supervised by the U.S.D.A. Soil Conservation Service (SCS). The dam was completed in 1968. The SCS office for Broome County, located at the Broome County Airport, has all design and construction information.

h. Normal Operating Procedures

Normal flows are discharged through the principal spillway. This structure has sufficient capacity to store and discharge a 100 year flood without use of the auxiliary spillway. Flow in excess of the 100 year storm will be discharged through the auxiliary spillway.

1.3 PERTINENT DATA

<u>a.</u>	Drainage Area (sq. mi.)	4.42
b.	Discharge at Dam (cfs)	
	Principal spillway at Maximum high water	160
	Principal spillway at auxiliary spillway crest elevation	132
	Reservoir drain at Normal water elevation	45
	Maximum known flood	43
	Total discharge at Maximum high water	17,500
c.	Elevations (USGS Datum)	
	Top of dam	1041.3
	Auxiliary spillway crest	1034.0
	Principal spillway crest	1016.0
	Low stage inlet	998.0
	Reservoir drain	981.9
d.	Reservoir (acres)	
	Surface area at top of dam	67.2
	Surface area at crest of auxiliary spillway	51.2
	Surface area at crest of principle spillway	24.1
e.	Storage Capacity (acre feet)	
	Top of dam	1280.
	Auxiliary spillway crest	905.
	Principal spillway crest	285.

. Dam

Type: Homogeneous earth fill, with keyed cutoff and drain parallel

to axis of dam.

Length (ft.) Slopes: upstream downstream

Crest Width (ft.)

1250. 3H to 1V 2.5H to 1V 20.

g. Principle Spillway

Type: Two stage reinforced concrete drop inlet structure. Low level orifice at elevation 998 and 15.0 weir at elevation 1016.0.

Weir length: Height 15. 35.

h. Auxiliary Spillway
Type: Grass lined channel having trapezoidal cross section.

Bottom Width Length Control Section 340. 50.

Reservoir Drain
 Type: 18 inch diameter cast iron pipe with reinforced concrece inlet.

control: Manually operated valve located in the spillway riser.

SECTION 2: ENGINEERING DATA

2.1 GEOLOGY

The Patterson, Brixius, Grey Creek Watershed Project Dam No. 1 is located in the glaciated portion of the "Appalachian Uplands" (northern extreme of the Appalachian Plateau) physiographic province of New York State. These uplands were formed by dissection of the uplifted but flat lying sandstones and shales of the middle and upper Devonian Catskill Delta. The plateau surface is represented by flat-topped divides with drainage generally southwest toward the Susquehanna River system.

Glacial cover is generally thin, although some north-south valleys are so thick that they are completely buried. The present surficial deposits have resulted primarily from glaciations during the Cenozoic Era, the last of which was the Wisconsin glaciation, approximately 11,000 years ago.

2.2 SUBSURFACE INVESTIGATION

A subsurface investigation was conducted by the Soil Conservation Service in 1965. This program consisted of 14 drill holes and 20 test pits at locations along the dam, auxiliary spillways, structural elements, and borrow area. Applicable subsurface information is included in Appendix F, Drawings #15 and 16.

In general, the soils in the vicinity of the dam are of glacial till or glacial lacustrine origin, and are silty gravel, clayey gravels, and sandy silts over shale bedrock. The permeability of these soils is low.

2.3 EMBANKMENT AND APPURTENANT STRUCTURES

The dam was designed and constructed under the supervision of the Soil Conservation Service. "As-Built" drawings of this dam are on file at the SCS office in Broome County. Selected drawings of the dam and appurtenances are included in Appendix F. The dam is composed of homogeneous earth fill, the maximum height of which is 65 feet, a cut-off trench having side slopes of l on l, and a foundation drain parallel to the axis of the dam near the downstream toe. A reinforced concrete riser serves as the principal spillway and a vegetated channel serves as the auxiliary spillway.

2.4 CONSTRUCTION RECORDS

Complete construction records are available from the SCS office in Broome County. No major construction changes were instituted.

2.5 OPERATION RECORD

Since the dam is an ungated floodwater retarding structure, no operating records are maintained regarding water levels. During periods of extreme rainfall, SCS personnel do monitor the reservoir.

2.6 EVALUATION OF DATA

The data presented in this report has been compiled from information obtained from Mr. Gary Page, Project Engineer for SCS in Broome County, and Mr. Donald Lake, Head of the SCS Design Section in Syracuse, New York. This information appears to be adequate and reliable for Phase 1 Inspection purposes.

SECTION 3: VISUAL INSPECTION

3.1 FINDINGS

a. General
Visual inspection of the Site #1 Dam was conducted on July 23, 1980.
The weather was cloudy and the temperature ranged in the low 70's.
The reservoir level at the time of the inspection approximately the invert of the low stage inlet of the service spillway riser (El.998.0).

b. Earth Embankment
No signs of distress were observed in connection with the earth embankment and no signs of misalignment, sloughing, seepage, subsidence, surface cracking or undesirable growth were noted. While no riprap was in use on the upstream slope for wave protection, no erosion was apparent. (See Photos #1 & 2)

Pedestrian and vehicular paths were noted on the crest and slopes of the embankment. These paths are a potential source of erosion. (Photos 5 & 6)

Near the downstream toe of the embankment on both sides of the impact basin erosion was evident. This erosion appears to be related to runoff from the embankment and the adjacent ball fields. (Photo #3)

Regrading in the area between the embankment and the auxiliary spillway was observed. A stockpile of soil was also evident near the outlet of the auxiliary spillway. Since no vegetation had been established on the regraded surface, erosion and slight ponding of runoff (from a previous storm) was noted. (Photo #5)

An internal drainage system composed of 2 - 8 inch diameter pipes surrounded by "drain fill" and extending parallel to the axis of the dam, provides drainage at the embankment-subgrade contact. These pipes exit through the concrete walls of the impact basin. Discharge from these pipes was 1 to 2 gpm each. The flow was clear. The animal guard on the left pipe was broken. (See Photo #3)

c. Service Spillway
The service spillway is generally in good condition. The maximum joint
extension of the pipe is 0.5 inches. The joint between the pipe and the
impact basin is open. The walls of the impact basin are slightly deteriorated.
Calcification was noted from a crack or cold joint on the upstream wall
about I foot above and to the right of the pipe. This area was dry at the
time of the inspection.

d. Auxiliary Spillway
The grass lined service spillway beyond the right abutment is generally in
good condition. Three ball fields were noted in the auxiliary channel, all
with removable fences. Vehicular paths and soil stockpiles were noted in
the channel. Vegetation was also evident on the slope between the auxiliary
spillway and the embankment. (Photo #7)

e. Reservoir Drain

The 18 inch diameter reservoir drain pipe and manually operated slide gate, controls of which are located atop the riser, is reported to be operational.

f. Downstream Channel

The downstream channel below the impact basin is ripraped. Some vegetation was observed along the banks of this channel. (Photo #4)

g. Reservoir

There are no signs of instability or sedimentation problems within the reservoir area.

3.2 EVALUATION

The problem areas observed during the inspection which require remedial measures are as follows:

- 1. Pedestrian and vehicular traffic has created paths and depressions on the slopes of the embankment, at the abutments and in the auxiliary spillway channel. This traffic must be eliminated, the depressions filled and the area seeded to prevent erosion.
- Erosion was evident near the toe of the embankment in the vicinity of the impact basin, at the right abutment, and between the auxiliary spillway outlet and the right abutment. These areas must be regraded and vegetation established as soon as possible.
- 3. Stockpiles of soil were observed in the auxiliary spillway channel and near the outlet of the channel. These stockpiles must be removed and the vegetation beneath the piles restored.
- 4. Recaulk the joint between the service spillway pipe and the wall of the impact basin.
- 5. The walls of the impact basin are slightly deteriorated and the left animal guard is broken. Repair the concrete surfaces of the impact basin and the animal guard.
- 6. Remove the vegetation on the slope between the right abutment and the auxiliary spillway channel, and along the banks of the downstream channel. Provide a program of periodic cutting and mowing of the dam and appurtenances. Also remove the debris in the approach channel of the auxiliary spillway.
- 7. Provide a program of periodic inspection and maintenance of the dam and appurtenances, including yearly operation and lubrication of the reservoir drain system. Document this information for future reference. Also develop an emergency action plan.

SECTION 4: OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

The normal water surface elevation is approximated by the low stage inlet of the service spillway. Downstream flows are limited by the 30 inch diameter service spillway pipe, except during extremely heavy runoff when the auxiliary spillway is in service. The dam provides 862 acre feet of flood storage between normal water level and the crest of the auxiliary spillway.

4.2 MAINTENANCE OF THE DAM

The dam is maintained by the County of Broome, New York. Maintenance of the dam is considered unsatisfactory as evidenced by the extensive vehicle and pedestrian paths which have initiated erosion on the slopes of the dam. In addition, erosion at the toe of the embankment near the impact basin and debris along the toe of the downstream slope were noted.

4.3 WARNING SYSTEM

There is no warning system in effect or in preparation.

4.4 EVALUATION

The dam and appurtenant structures have not been maintained in satisfactory condition as noted in "Section 3: Visual Inspection."

SECTION 5: HYDROLOGIC/HYDRAULIC

5.1 DRAINAGE AREA CHARACTERISTICS

The drainage area above the Patterson Brixius Site 1 dam is 2829 acres or 4.42 square miles. **Delin**eation of the watershed was made using the USGS 7.5 minute quadrangle, Maine, New York. The watershed consists of woodlands and some residences in a primarily rural setting. Relief ranges from moderate to fairly steep.

5.2 ANALYSIS CRITERIA

The analysis of the spillway capacity of the dam and storage of the reservoir was performed using the Corps of Engineers HEC-1 computer model. The unit hydrograph was defined by the Snyder Synthetic Unit Hydrograph method, and the Modified Puls routing procedure was incorporated. The Probable Maximum Precipitation (PMP) was 21.0 inches (24 hrs., 200 sq. mi.) from Hydrometeorological Report #33 in. accordance with recommended guidelines of the Corps of Engineers. The floods selected for analysis were 20, 40, 50, 60, 80, and 100% of the Probable Maximum Flood (PMF) flows. The PMF inflow of 7082 cfs was routed through the reservoir with no significant attenuation.

5.3 SPILLWAY CAPACITY

The spillway is a reinforced concrete drop inlet structure, 35 feet in height. It creates a weir length of 15 feet at elevation 1016.0, approximately 25. feet below top of dam. At auxiliary spillway crest elevation it has a capacity of 132 cfs. At top of dam, the service spillway and auxiliary spillway have a total capacity of 17,500 cfs.

5.4 RESERVOIR CAPACITY

The reservoir capacities at the crest of the spillway and the top of dam are 285 and 1280 acre feet respectively. Surcharge storage from spillway crest to auxiliary spillway crest and auxiliary spillway crest to top of dam are 2.63 and 1.59 inches of runoff.

5.5 FLOODS OF RECORD

The highest known water elevation was 1026.2 or 10.2 feet above the low level orifice (not yet reaching the service spillway crest). This occured during September 1975, the estimated outflow of this storm is 95 cfs.

5.6 OVERTOPPING POTENTIAL

The maximum capacity of the spillways is 17,500 cfs before overtopping would occur. This capacity passes the full PMF inflow of 7,083 cfs with 3 feet freeboard. The routed 1/2 PMF outflow is 3,457 cfs.

5.7 EVALUATION

The spillway has a capacity to pass the total PMF and attenuate storm of greater frequency.

SECTION 6: STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

No signs of distress were observed in connection with the earth embankment.

b. Design and Construction Data

A stability analysis was conducted by SCS during the design of the dam. The analyses were performed using the modified swedish circle method. The soil parameters assumed were γ_d = 122.8, γ_m = 137.0, γ_s =140.5, γ_b =78.0, ϕ = 270 c = 300. The results of these analyses are as follows:

Condition

Minimum Factor of Safety

1.	Upstream slope	= 1:3, full	draw down	1.45
	15' berm at el.	1006 & 10'	bern at el. 995	• • •

Downstream slope = 1:2.5, drain at c/b = 0.6
 1.58

The calculated factors of safety for this dam are in excess of the minimum factors recommended by the Corps of Engineers. The dam is, therefore, considered to have adequate factors of safety for stability. Further information concerning this analysis is included in Appendix E.

c. Post Construction Changes

No post construction changes were initiated. Removable fences for sporting activities have been installed in the auxiliary spillway.

d. Seismic Stability

The dam is located in Seismic Zone 1. Therefore, a seismic analysis is not warranted.

SECTION 7: ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

The Phase I Inspection of the Patterson Brixius Grey Creek Watershed Project Site 1 Dam did not reveal conditions which constitute a hazard to human life or property. The earth embankment is not considered to be unstable and appears capable of retarding floodwaters resulting from the PMF.

b. Adequacy of Information
The information reviewed appears adequate for Phase I Inspection purposes.

c. Need for Additional Investigation
No additional investigations are required at this time.

d. Urgency Within I year of notification to the owner, the following remedial measures must be completed.

7.2 RECOMMENDED MEASURES

- 1. Eliminate the pedestrian and vehicular traffic on the embankment and auxiliary spillway, backfill all depressions and reseed these areas.
- 2. Repair the erosion and reseed the areas adjacent to the impact basin, at the toe of the right abutment, and the regraded area between the right abutment and the outlet of the auxiliary spillway. Also remove the stockpiles of soil in the auxiliary spillway channel and channel outlet, and reseed.
- 3. Recaulk the joint between the service spillway pipe and the impact basin wall. Repair the concrete surfaces of the impact basin, and repair the left animal guard.
- 4. Remove the vegetation along the left slope of the auxiliary spillway and on the banks of the downstream channel. Remove the debris in the approach channel of the auxiliary spillway. Provide a program of periodic cutting and mowing of the dam and appurtenances.
- 5. Provide a program of periodic inspection and maintenance of the dam and appurtenances, including yearly operation and lubrication of the reservoir drain system. Document this information for future reference. Also develop an emergency action plan.

APPENDIX A

PHOTOGRAPHS

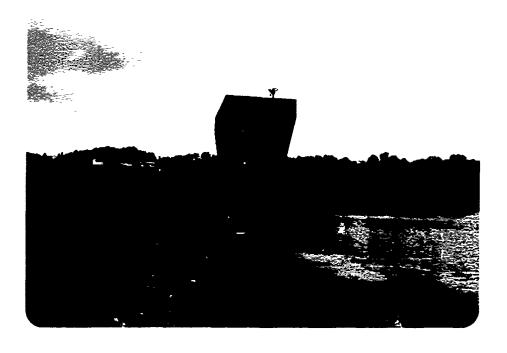


Photo #2 Upstream Slope & Riser

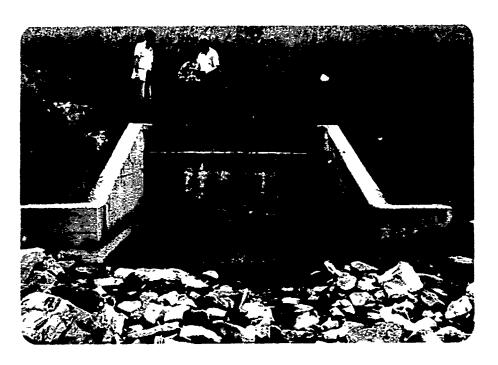


Photo #3 Impact Basin



Photo #4 Downstream Channel



Photo #5 Downstream Area Viewed from Crest



Photo #6 Downstream Face - Left Abutment



Photo #7
Auxiliary Spillway & Right Abutment

APPENDIX B

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1)	Ras	sic Data
-,	a.	General
	a.	Name of Dam Patterse, Birries Great Cisk Site!
		Fed. I.D. # NY 698 DEC Dam No. 86 B 3457
		River Basin Susquehanna
		Location: Town Vn.co County Bicome
		Stream Name Patterness Crack
		Tributary of Sugarburne Rivie
		Latitude (N) 4 6 8 2 Longitude (W) 76 1.3
		Type of Dam Early Emberka
		Hazard Category c" High
		Date(s) of Inspection
		Weather Conditions Clarky Les 70's
		Reservoir Level at Time of Inspection Appear Low State Intel (61. 998 0)
	b.	Inspection Personnel Janic C Variet, R. P. McCarly
-	c.	Persons Contacted (Including Address & Phone No.)
		Gong Page - Paged Egr, SCS Bighander
		(C7-773-275! Breeze Ca. Broken Broken L.
		12 1/2 Lake 315 423 - 5505 5yours 505
	d.	History:
		Date Constructed :568 Date(s) Reconstructed
		Designer Sei Consider Service
		Constructed By RD Ballagla, Cop.

Owner Brown County N.Y.

)	Emb	ankme	<u>nt</u>					
	a.	Char	acteristics					
		(1)	Embankment Material Slacial fill					
		(2)	Cutoff Type enth					
	٠	(3)	Impervious Core					
		(4)	Internal Drainage System 28" diem cmp					
		(5)	Miscellaneous					
			•					
	b.	Cres	t .					
		(1)	Vertical Alignment <u>900</u>					
		(2)	Horizontal Alignment <u>900 d</u>					
		(3)	Surface Cracks					
•			·					
		.(n)	Miscellaneous b.ke and vahicular parks en cres					
			slight depressions resulting					
	c.	Upst	ream Slope					
		(1)	Slope (Estimate) (V:H)1:3					
		(2)	Undesirable Growth or Debris, Animal Burrows					
		(3)	Sloughing, Subsidence or Depressions depressions (5:(1))					
			Jean voliceter & podestiian travel.					
		,						

resulting from podes him & web. culor deaffice eres, on near too ad impositors in (bold sides) from bullfield (4) Surface Cracks or Movement at Toe	5)	Surface Cracks or Movement at Toe unchsenable
Undesirable Growth or Debris, Animal Burrows Compared Compare	own	stream Slope
3) Sloughing, Subsidence or Depressions	1)	Slope (Estimate - V:H) 1:7.5
Sloughing, Subsidence or Depressions	2)	Undesirable Growth or Debris, Animal Burrows
resulting from podes him & web. culor draffic eres. on near too ad impact basin (bold sides) from trillfield Surface Cracks or Movement at Toe		
resulting from podestrian & vehicular direction directio	(3)	Sloughing, Subsidence or Depressions depressions (slight)
Surface Cracks or Movement at Toe		resulting from podestion & ushicular traffic
(5) Seepage		wissin near too at impost basin (both sides) from tall field
(6) External Drainage System (Ditches, Trenches; Blanket) 10 10 10 10 10 10 10 10 10 10 10 10 10 1	(tt)	Surface Cracks or Movement at Toe
(7) Condition Around Outlet Structure eresion on bolk sides of upstime intil don to intell along to a fire bill fields	[5)	Seepage nca
upstion wall don to remail along the of for bell fields	(6)	External Drainage System (Ditches, Trenches; Blanket)
upsion wall don to remail along the of for bell fields	, m, n	
	./)	Condition Around Outlet Structure ecoson on both sides of
	8)	

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		(1.)	Erosion at Contact eresion way to four right and = 60 tok
			bien races ingrating; area ragnoled & large pole of soil billy
		(2)	Secnage Along Contact - nene
			num outhed of auxiliary spilling between tien of abt (right)
			so - porded that at too our tall field for previous rain also some
			eros en in regnit d'araci
3)	Dwa	: n	
.) j			e System
	a.		eription of System 8 cmp parallel to axis e) dam & colletting
		- 12	valle of in pact basin
	b.	Cond	lition of System good - an mal good in left pipe
			orcken
	c.	Disc	charge from Drainage System Appea 1 to 2 gpm line est
			ac .
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41)			entation (Momumentation/Surveys, Observation Wells, Weirs, eters, Etc.)
٠.			p c ale

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	c.	Condition of Auxiliary Spillway generally good - bull fields
		in siepail sactions we remove the pencas - soil pile - & benches
		Jane debris in approach channel.
		vegetation en reproped stopen between aux et right abot.
	d.	Condition of Discharge Conveyance Channel
		good: pedasilmen duehiculen palls in
		gextient cheme! have contact deposes in
8)	Res	ervoir Drain/Outlet •
		Type: Pipe > Conduit Other
		Material: Concrete Metal Other
		Size: Length
		Invert Clevations: Entrance Exit
		Physical Condition (Describe): Unobservable
		Material:
٠,		Joints: Alignment
		Structural Integrity:
		Hydraulic Capability:
		Means of Control: Gate Valve Uncontrolled
		Operation: Operable Other
		Present Condition (Describe):

9)	<u>Structural</u>								
	a.	Concrete Surfaces gamally good							
		som slight delocionalier of impact bases walls							
	b.	Structural Cracking							
		1							
	c.	Movement - Morizontal & Vertical Alignment (Settlement)							
		Laoliva 200							
	d.	Junctions with Abutments or Embankments							
		ad equate							
		·							
	e.	Drains - Foundation, Joint, Face كريم دومات							
٠٠.									
	f.	Water Passages, Conduits, Sluices <u>good ecodilica</u>							
		·							
	g.	Seepage or Leakage now todand							
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nergy	Dissipators (Plunge	Pool	etc.)		···	
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APPENDIX C

HYDROLOGIC / HYDRAULIC

ENGINEERING DATA AND COMPUTATIONS

CHECK LIST FOR DAMS HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

AREA-CAPACITY DATA:

	,	Elevation (ft.)	Surface Area (acres)	Storage Capacity (acre-ft.)
1)	Top of Dam	1041-3	67.8	1890
2)	Design High Water (Max. Design Pool)	1038.0	60.2	10:9
3)	Auxiliary Spillway Crest	1034.0	51.2	915
4)	Pool Level with Flashboards	•		
5)	Service Spillway Crest	1016.0 998.0 (loskal	<u> 24.1</u> 'onluc)	285

DISCHARGES

		(cfs)
1)	Average Daily	10.
2)	Spillway @ Maximum High Water	160
3)	Spillway @ Design High Water	152
4)	Spillway @ Auxiliary Spillway Crest Elevation	_132_
5)	Low Level Outlet	15'
6)	Total (of all facilities) @ Maximum High Water	17,500
7)	Maximum Known Flood	
8)	At Time of Inspection	4 1/2.

CREST:		ELEVATION: 1941-3	
Type: hand g	en couth fell		
Width: 3	Length	: <u>1850</u>	
Spillover drop	for , right abouture	Lund chrim	no l'avguirre
Location	for , right about me	-st	·
SPILLWAY:			
SERVICE		ΛυχΙΙ	JINRY
1916.	Elevation	1034.	
drop inlet	Туре	grees here	d chansel
2.5 x 7.5 '	Width	340'	
	Type of Control		
	Uncontrolled		
	Controlled:		
	Type . (Flashboards; gate)		·
	. Numb‡r		
	Size/Length		
	Invert Material	Vigetated	
	Anticipated Length of operating service	9 kis	,
316 contact	Chute Length		
	Height Between Spillway (Crest <u> </u>	1/0

Type: Alar	
Location:	
Records:	
Date -	
Max. Reading	
FLOOD WATER CONTROL SYSTEM:	
Warning System: Novie	
Method of Controlled Releases (mechanisms)	

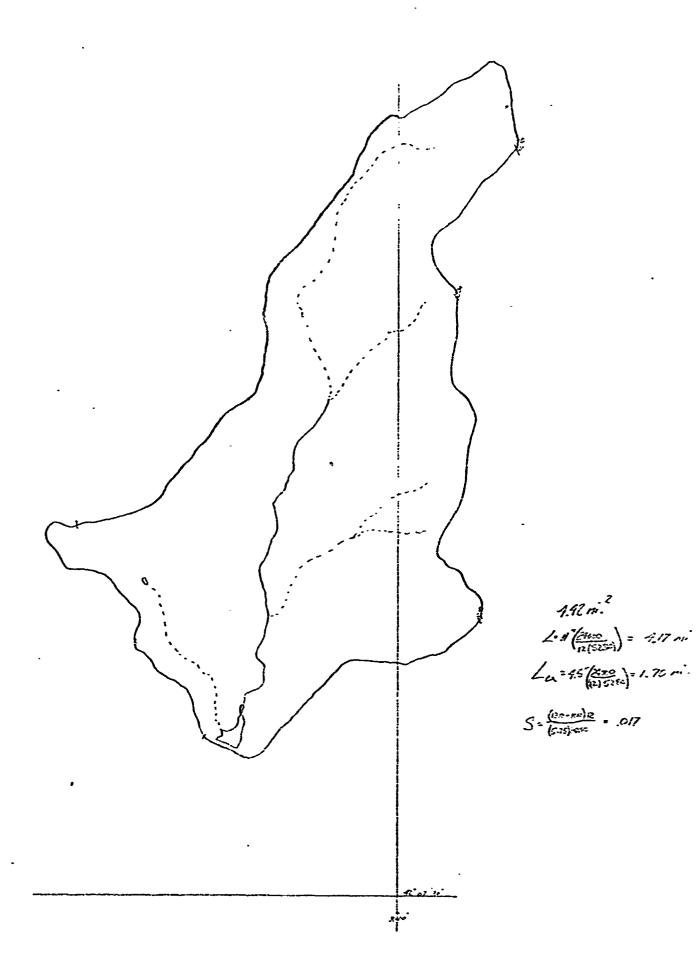
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DRAINAGE AREA: 112 mi.	
DRAINAGE BASIN RUNOFF CHARACTERISTICS:	
Land Use - Type: Some deploper to sall with how the	7910
Terrain - Relief: 10kints to stop stops	-
Surface - Soil: 101 prince belif	-
Runoff Potential (existing or planned extensive alterations to existing (surface or subsurface conditions)	
fish i moll portential - chock - bu sory.	
hit i molt potential - chore-busing.	
Potential Sedimentation problem areas (natural or man-made; present or futu	ıre)
Potential Backwater problem areas for levels at maximum storage capacity including surcharge storage:	
Dikes - Floodwalls (overflow & non-overflow) - Low reaches along the Reservoir perimeter: Location: ////E	
Elevation:	
Reservoir:	
Length @ Maximum Pool	
Length of Shoreline (@ Spillway Crest) 11.00 //- (Miles)	

PARTETER - BROYLUS TITE Nº 1 1.12 mi. DA. 6 = 4.17 mi. Co = 1.70 mi Ct = 2.0 or slightly lower due to steepwess tp = G (L x Lax) 0,3 = 2.0 (1.17 x 1.70) = 3.6 hrs. tr = tp : 36 = 0.65 Tp= tp = 0.5 (tr) = 3.925 kr. .Cp= 0.625 Timeral : Pero (1818 23) 21.0" \$ 111 123

133 112 Spling Preserve Carectures: Ec (SCE) Q(ds) = 60 Ft.) most of critice 993 0 43,4 pline. So we little 10160 285.0 50 inery " crest 1034.0 905.0 132 dergo high & 1069.0 1033.0 6210 1 of Din 1091.3 1280.0 17500

1=1250' C= 3.0



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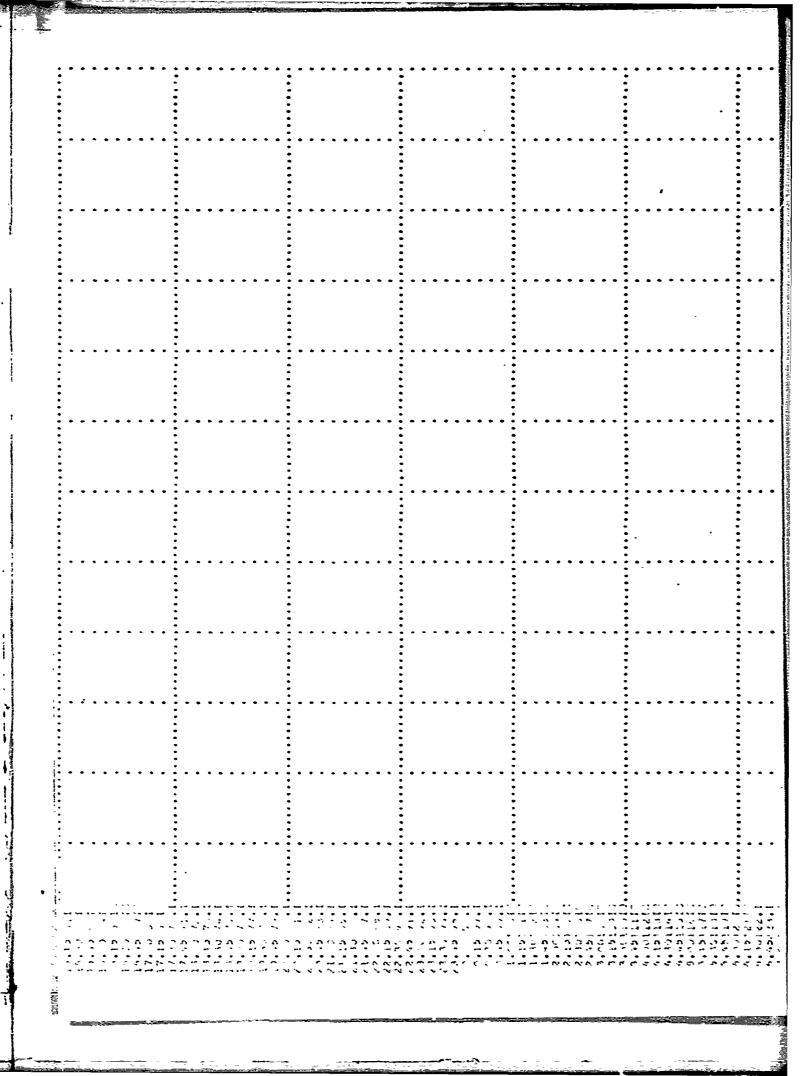
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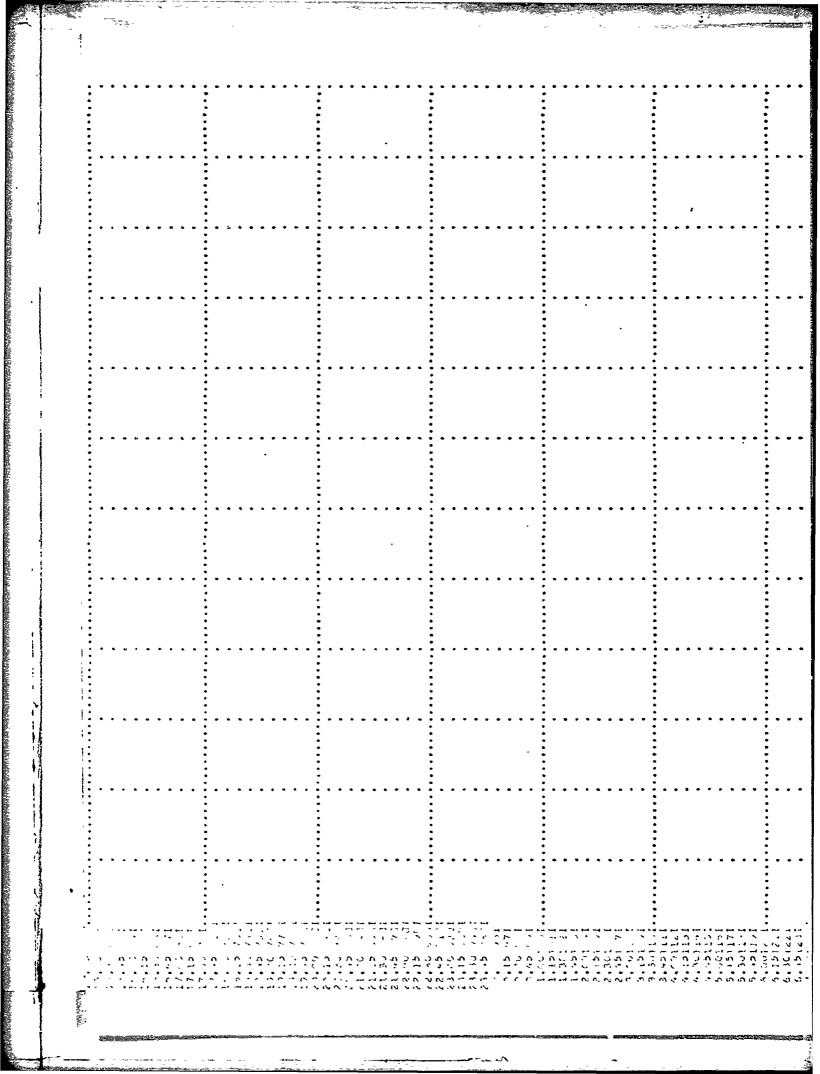
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APPENDIX D

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- 2) Soil Conservation Service, <u>National Engineering Handbook</u>, Section 4, Hydrology, August 1972 (U.S. Department of Agriculture).
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APPENDIX E

STABILITY ANALYSIS

Memorandum

TO: W. S. Aukinson, State Consertation DATE: April 20, 1965 Engineer, SCS, Syracuse, New York 13210

FROM: Rey S. Decker, Head, Soil Mechanics Laboratory, SCS, Lincoln, Nebraska 68508

SUBJECT: ENG 22-5, New York WP-08, Patterson Creek, Site No. 1 (Broome County)

ATTACHMENTS

- 1. Form SCS-354, Soil Mechanics Laboratory Data, 1 sheet.
- 2. Form SCS-355, Triaxial Shear Test Data, 1 sheet.
- 3. Form SCS-352, Compaction and Penetration Resistance Report, 4 sheets.
- 4. Form SCS-353, Grain Size Distribution Graph, 1 sheet.
- 5. Form SCS-357, Summary Slope Stability Analysis, 2 sheets.
- 6. Investigational Plans and Profiles.

DISCUSSION

FOUNDATION

A. <u>Classification</u>: The foundation conditions and materials at this site are clearly outlined and well depicted in the geology report.

The abutments consist of till that is logged as a dense to very dense GM. This till contains approximately 15 percent material larger than 3 inches with numerous cobbles and flags larger than 6 inches.

The emergency spillway samples 65W2618, 65W2619 and 65W2620 are representative of the till at the surface on the abutments. Samples from the emergency spillway contain slightly less than 50 percent fines and are classed as GC.

The materials in the floodplain section consist of a dense till overlying gravels and silts of lacustrine origin. The lacustrine sediments in turn overlie a dense glacial till.

The surface till zone is about 8 feet thick. This material contains approximatery 60 percent gravel and 20 percent fines. Iaboratory sample 65W2617 is representative. The lacustrine gravels range from a few feet thick to 10 feet thick. Field samples indicate that these materials contain from 30 to 60 percent material passing the No. h sieve and from about 10 to 20 percent fines. The lacustrine silts contain approximately 90 percent fines. The till in the surface zone is classed as a GC-GM.

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Gradation curves for the lacustrine materials are included in the geology report.

B. Blow Count: Blow count in the surface till zone was generally above 30 blows/foot. Tests in the surface couple feet in DH-3 and DH-4 showed blow counts of 19 and 13 blows, respectively. The material in this zone is logged as moist to wet but a water table is not indicated.

The lacustrine material below the surface till zone has blow count values ranging from 36 to more than 100 blows/foot on centerline. The ML zone in Test Hole 302 downstream from centerline had blow counts in the range of 15 to 19 blows/foot. The materials within the lacustrine zone are generally logged as wet and seepage was noted in some locations.

C. Shear Strength and Consolidation: Undisturbed samples were not submitted. The blow count data indicated a relatively strong foundation with a low consolidation potential for the loading range planned.

The fine fraction of these materials is somewhat plastic and blow count could possibly be lower if the moisture content was not near theoretical saturation at the time of test.

D. Permeability: With the exception of the GW in the rottom of the channel, the permeability of the foundation material is expected to be relatively low for each class of material. The lacustrine gravel is expected to be the most pervious material other than the stream channel gravels. The D₁₀ size of the lacustrine gravel is about 0.07½ mm. or less. The blow count indicates a relatively dense gravel; therefore, we estimate the permeability rate will be in the range of 1 to 5 feet per day or less, depending upon the amount of fines.

EMBANKMENT

- A. Classification: The embankment material will come from the emergency spillway. Three samples were submitted from the spillway. The samples indicate that the till from the spillway is very uniform. It contains slightly less than 50 percent fines and is classed as a GC. The liquid limit is near 30 and the PI is about 12. About 15 percent of the material is larger than the 3-inch size.
- B. Compacted Descript: Standard Proctor compaction tests were made on the three samples submitted. The tests were made on the fraction finer than 3/4 inch in accordance with ASTM D-698T, Method C. The maximum density obtained was 125 p.c.f. for all three samples.

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A standard Proctor test was made on the minus No. 4 fraction of Sample 65W2619 for correlation purposes. The density obtained was 119 p.c.f. Based on the density and the percent of the material larger than the No. 4 sieve size included in the compaction sample for the minus 3/4-inch test, computations show that the density of the minus 4 fraction within this test sample was also 119 p.c.f. This indicates that the gravel fraction did not interfere with compaction of the minus 4 fraction in the 1/30 cubic foot compaction mold.

C. Shear Strength: A triaxial shear test was made on Sample 65W261). The test was made on the minus 3/4-inch fraction at a density of approximately 98 percent of standard Proctor. A consolidated, undrained test was made and pore pressure was measured during the test. The effective stress shear strength values obtained were $\emptyset = 27^{\circ}$, c = 300 p.s.f. and the total stress shear values obtained were $\emptyset = 19^{\circ}$, c = 325 p.s.f.

The test values are considered r presentative of the borrow materials for a placement density of 98 percent of standard Proctor and are suggested for design.

SLOPE STABT. ITY

Slope stability was checked with a modified Swedish circle method of analysis. The analysis was made on the maximum embankment section and the trial failure arcs were limited to the embankment only.

A phreatic line was assumed from emergency spillway elevation to a drain at c/b = 0.6.

The analysis shows that the proposed 2 1/2:1 downstream slope with a drain has a factor of safety of 1.58.

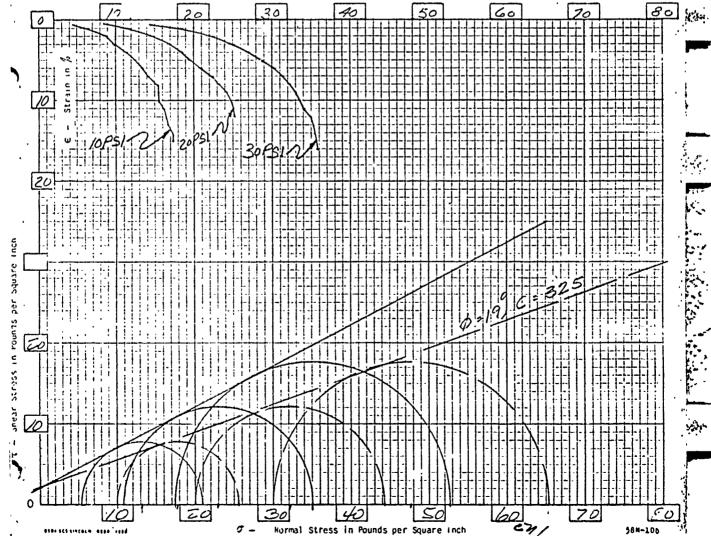
A 3:1 upstream slope with a 10-foot berm at elevation 995 has a factor of safety of 1.36 with complete rapid drawdown considered. The addition of a 15-foot berm at elevation 1006 plus the 10-foot berm at elevation 995 results in a factor of safety of 1.48, which is very near the suggested minimum of 1.50 when effective stress shear parameters are used in the analysis.

SETTLEMENT ANALYSIS

The consolidation potential is expected to be low. The foundation conditions appear to be uniform and differential settlement is not expected to be a problem. The channel banks are near vertical in some places, however, and some differential might occur in this area.

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RECOMMENDATIONS

A. Site Preparation: Normal site preparation should be adequate to remove any loose materials at the surface.

We recommend that the channel banks be flattened to insure a good bond between the backfill and the foundation and to reduce the possibility of critical differential settlement in this area.

B. <u>Cutoff</u>: The Geologist suggested a shallow cutoff trench. We concur with this suggestion. A minimum trench depth of about 5 feet is suggested to insure that the trench bottoms below the zone affected by roots, rodents, cracking, etc.

The trench backfill may consist of GC material from the emergency spillway. The backfill should be compacted to a minimum of 98 percent of standard Proctor density.

C. Principal Spillway: The proposed principal spillway location is at \$\frac{4}{5}\text{station 8+00}\$. The foundation material at this location consists of till upstream from centerline. Downstream from centerline the foundation contains about a 4-foot zone of lacustrine silt and sand between layers or zones of till. The blow count within the lacustrine silt ranges from 15 to 19 blows per foot and blow count below the surface foot or two in the till is in excess of 30 blows per foot.

The conduit will be bedded in dense till and dense lacustrine silts. The consolidation potential is expected to be low and no unusual problems are anticipated.

Rased on blow count, permeability is expected to be low. If zones or stratum of pervious materials are encountered in the lacustrine materials, it might be desirable to encompass the conduit with a filter drain.

The Geologist points out that the material at grade is erodible.

Drain: A drain is recommended to control the phreatic line in the embankment and to provide a safe outlet for underseepage. A trench drain with a pipe outlet is suggested. We concur with the trench depths suggested in the geologic report. At these depths the trench will bottom in the most pervious zones. The trench depths suggested are as follows:

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T.P.	Suggested Trench Depth	Material at the Trench Bottom Logged As
508	6 feet	Till
503	5 feet	Till
302	12 feet	'SM with gravel streaks
502	14 feet	SM with gravel streaks
501	14 feet	SM with gravel streaks
504	12 feet	SM .
509	8 feet	GM-GW

The suggested filter limits are shown on the attached Form SCS-353. The suggested limits are such that ASTM No. 78 road gravel may be used.

Embankment Design: Ε.

- Placement of Material. The borrow materials consist of a uniform glacial till from the emergency spillway; therefore, a homogeneous embankment is recommended. The borrow material should be placed at a minimum of 98 percent of standard Proctor density with the control based on the minus 3/4-inch fraction. The placement moisture content should be slightly wet of optimum.
- Slopes. The proposed 2 1/2:1 downstream slope has an acceptable factor of safety and is recommended. The proposed 3:1 upstream slope with a 10-foot berm at elevation 995 requires modification to obtain an acceptable factor of safety. The stability analysis shows that the addition of another berm 15 feet wide at elevation 1006 results in a factor of safety of 1.48. This addition or a comparable modification is recommended.
- Settlement. An overfill allowance of 1.5 feet is suggested to compensate for residual consolidation within the fill and foundation.

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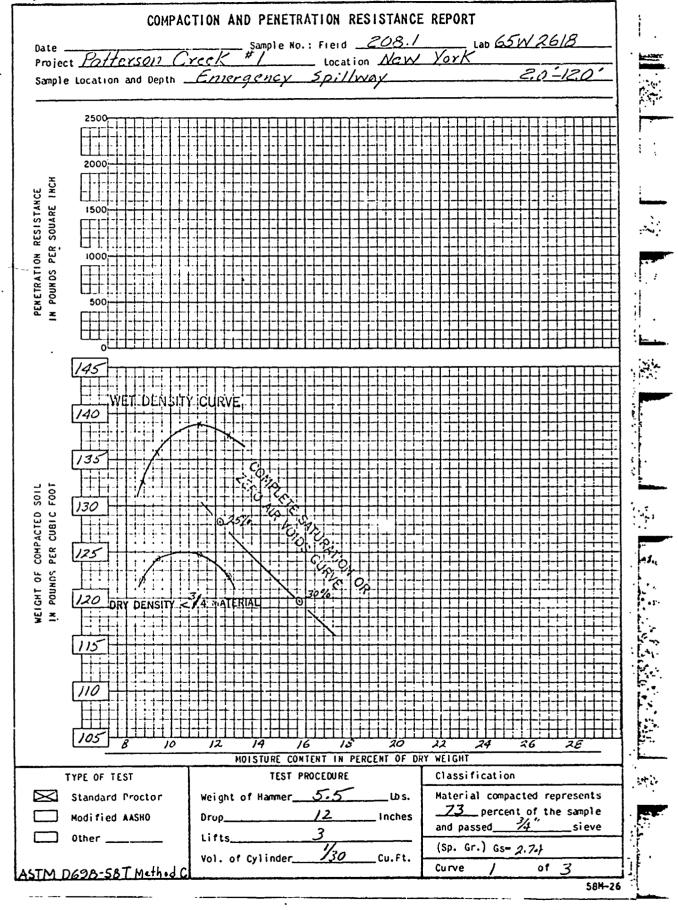
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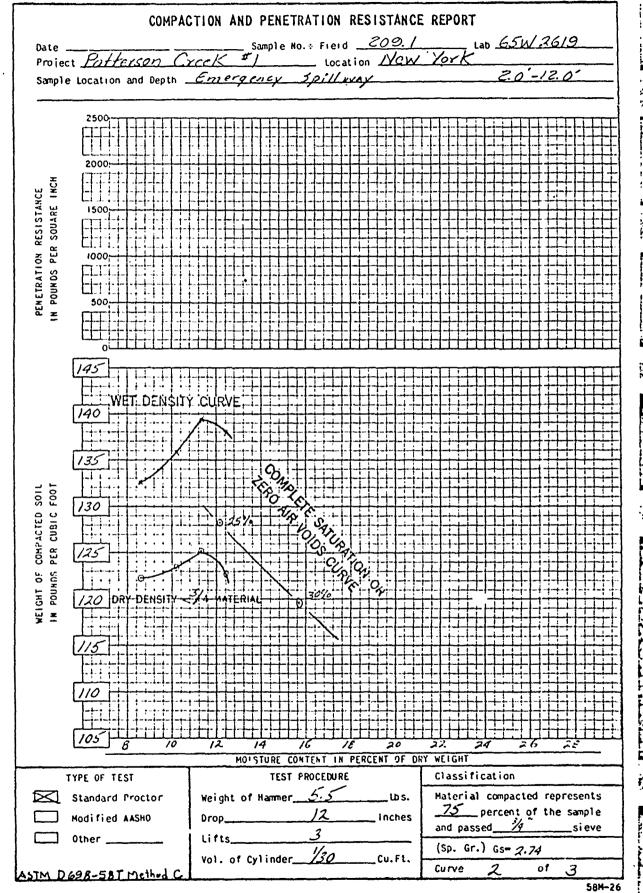
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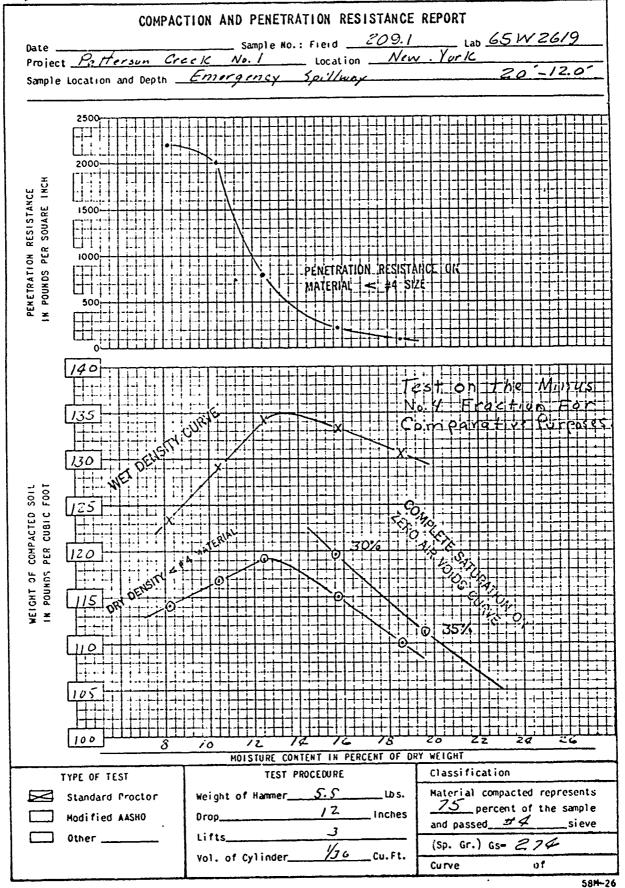
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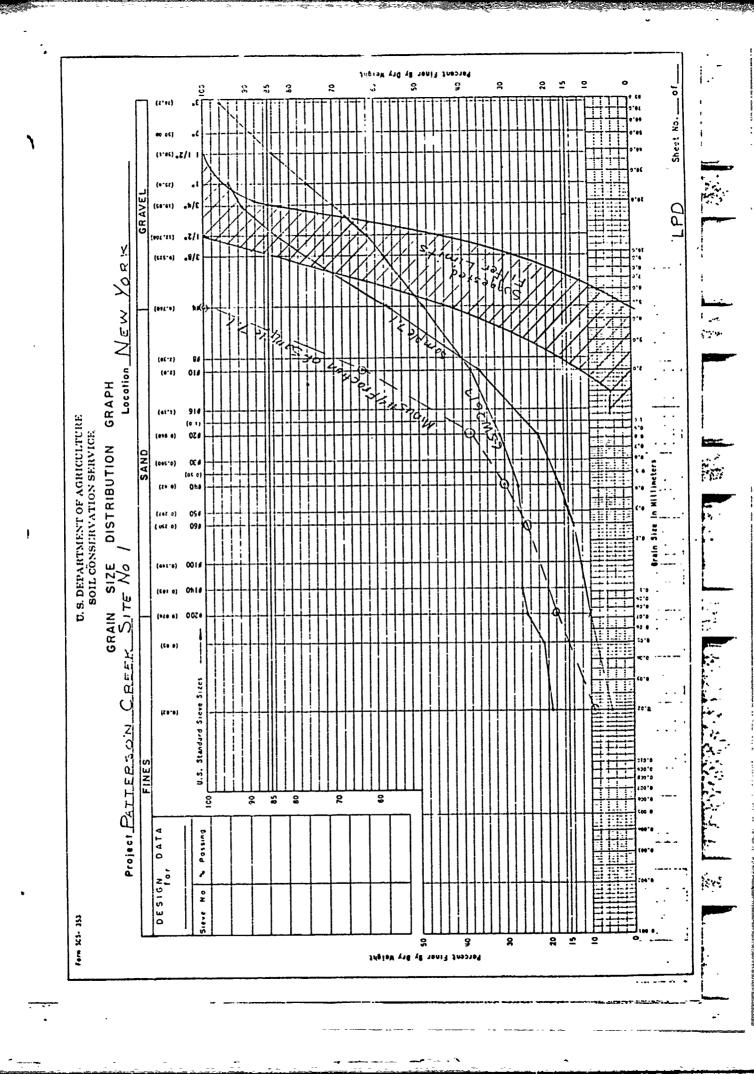


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Date .	ct <i>Patterson</i> (Samp	ole do Freid .	210.1	Lab £	55W2620
Projec	ct Patterson (reck #/	Locati	on New	York	
Samp1	e Location and Depth _	Emergen	cy spilling	<u> </u>	 	2.0-12,0
				······································		
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	140 WET DENSITY	CURVE				
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8 5 8 5	130		3			
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COMP.	125		6,2			
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913M			0 30%			
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-0			RE CONTENT IN PE	RCENT OF DE		
	TYPE OF TEST	i	TEST PROCEDURE		Classificati	
\boxtimes	Standary Proctor	Į.	mer	Lbs.		ppacted represents cent of the sample
<u>ا</u>	Modified AASHO	Drop	<u> 12</u> 3	Inches		<u>3/4</u> sieve
نا	Other	Vol. of Cylin		Cu. 5.	(Sp. Gr.) G:	s= <i>2.13</i>
ASTM F	0698-58T Melhod C	voi. of Cylii	nuer	Cu.ft.	Curve 3	of 3
		······································				58H-26





FORM SCS-357 10-58

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

Speel 10/2

SOIL MECHANICS LABORATORY 1/22

Bramam Section

SUMMARY - SEUTE STABILITY ANALISTS
State NEW YORK Project PATTERIAN CREEK SITE #1
Date 4-13-45 Analysis Made By 67.67 A.M. Checked By A.M. A. F
Method of Analysis SMITHISH CIRCLE

Location of Material							E) 997 G	5-6		
Sample No.		_						2419		
7 d								2.8		
7 m								7.0		
₹ s							14	10.5		
7 b								75.0		
Condition	Opt.	Sat.	Opt.	Sat.	Opt.	Sat.	Opt.	Sat.	Opt.	Sat.
ф								27.0°		
Tan 🏚							CU	2.510		
К										
С								320		

		UPSTREAM SLOPE"	
Trial	Slope	Conditions	Fs
	311	Fulling udown - 10 horm soler 935-Frecht	
		from one, sollie thra Emp (27.0-300)cm/y	1.3%
1,4	311	Sme's HI except 15 her in delev. 1006 \$ 10 here	
		20/04 295,0	1.43
2	3:1	Full drindown-15 herm relex 1025 f 12 herm relex	
		995-4recut from son shier then End (27.0°-304)	
		anly //	1.5%
_3	3:1	Tillderedown -15 comecle 12 1 d 16 hor miseie 995	
		Lyon theom on ship to a Ford 577-810) into	1.15
1	3:1	Filldry adownto remachen 1206 \$11 'con . Solow 995	
		Are cutfrem con star the Employe = 33) only	1.23
		//	

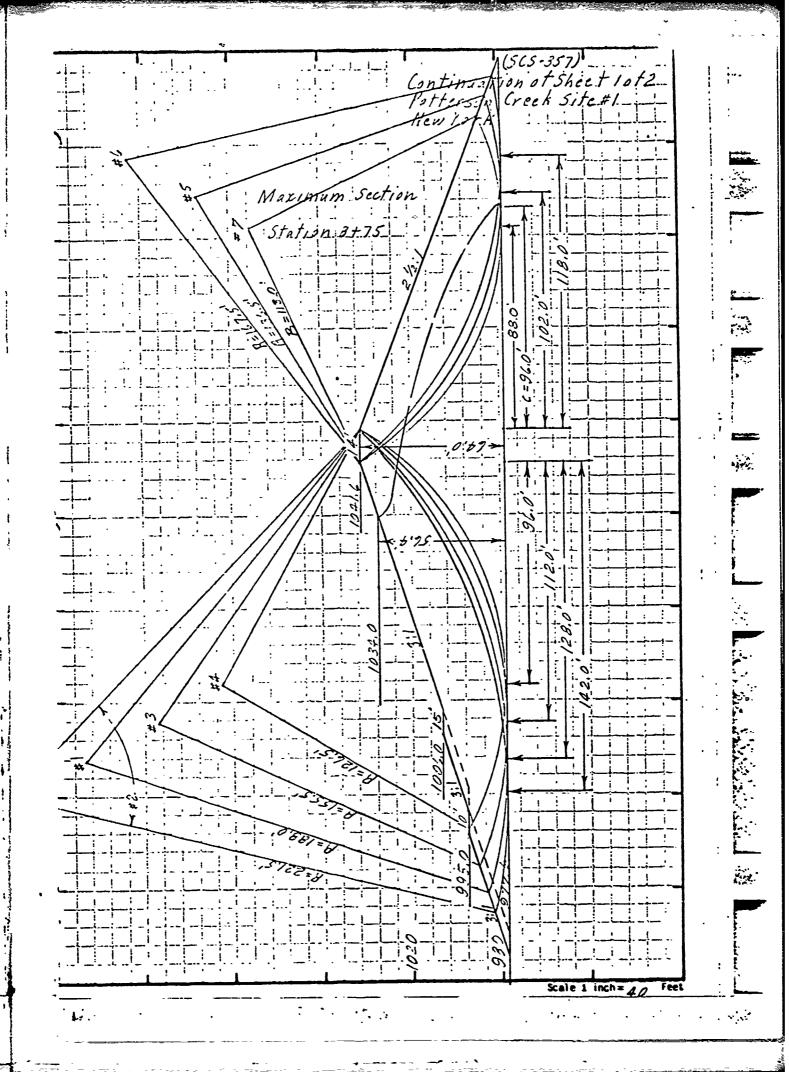
		DOWNSTREAM SLOPE	
Trial	Slope	Conditions	Fs
	215:11	Propo a 1/2 = 0.6 - Na harm-Are out from one shills	
		the Indiagnoscoloph,	1.53
	23:1	Promatheras-Noberm recent from no - 1744	
		11, 1. Fp. 6/27 2: 300) 01.1.	1.62
2	22:1	Dring @ 9/6 = O. 6 - No corn - Are cut from	
		you solde thru emb (27:-300) only.	1.50
 			
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		Note - Sat. shear values anly.	
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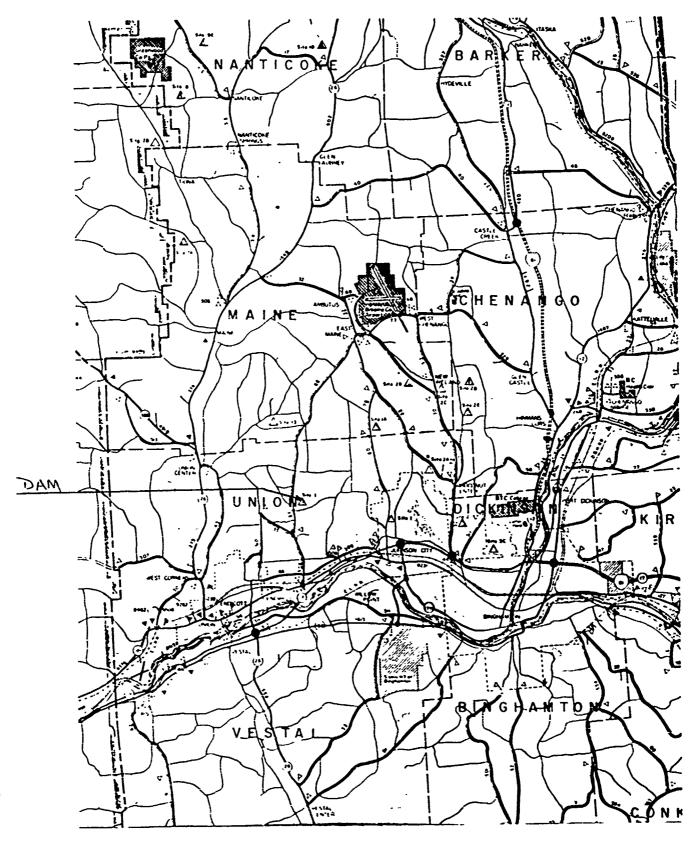
To be used to report to field offices data used for slope stability analyses and the results of the analyses. The right side of the form will be used for a sketch of the embankment on which the analyses have been made.

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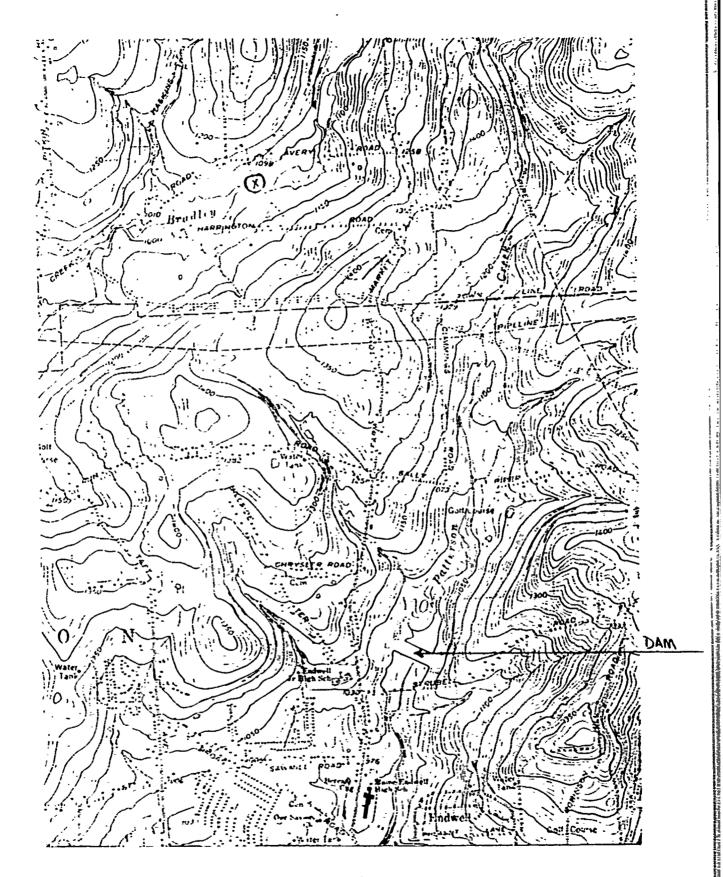


APPENDIX F

DRAWINGS



VICINITY MAP



TOPOGRAPHIC MAP

PATTERSON BRIXIUS & GREY CREEK WATERSHED PROJECT

FLOODWATER RETARDING DAM, NO. I

DRAINAGE AREA
TOTAL STORAGE
TO EMERGENCY SPILLWAY CREST WATER SURFACE AREA
AT SEDIMENT POOL
HEIGHT OF DAM
VOLUME OF FILL

2829 ACRES
905 ACRE FT.
7.6 ACRES
65 FEET
23,500 CUBIC YARDS

BUILT UNDER THE WATERSHED PROTECTION AND FLOOD PREVENTION ACT

BY

COUNTY OF BROOME
WITH THE ASSISTANCE OF THE
SOIL CONSERVATION SERVICE
OF THE
U.S. DEPARTMENT OF AGRICULTURE

1965 :---

INDEX

SHEET I - COVER SHEET

SHEET 2 - PLAN OF STORAGE AREA

SHEET 3 - PLAN OF DAMSITE

SHEET 4 - PROFILE ALONG & OF DAM

SHEET 5 - PROFILES

SHEET 6 - DRAINAGE DETAILS

SHEET 7 - DRAINAGE DETAILS

SHEET 8 - PLAN - PROFILE OF PRINCIPAL SPILLWAY

SHEET 9 - RISER - STRUCTURAL DETAILS

SHEET 10 - RISER - REINF STEEL DETAILS

SHEET II - CRADLE, ANTI-SEEP COLLARS AND STE

SHEET 12- POND DRAIN INLET DETAILS

SHEET 13 - IMPACT BASIN

SHEET 14 - TRASH RACKS, AND MISC. DETAILS

SHEET 15 - LOGS OF TEST HOLES

SHEET 16 - LOGS OF TEST HOLES

GREY "CREEK" **OJECT**

DAM, NO. 1

2829 **ACRES** 905 ACRE FT.

...7 56 ACRES

FEET 65

CUBIC_YARDS 3,500

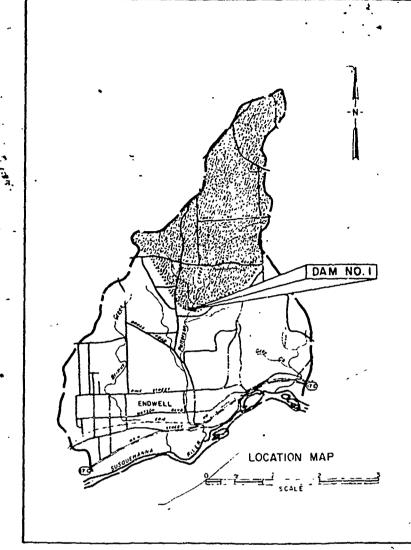
ROTECTION AND

ACT

ME F THE RVICE

CULTURE

- 9 RISER STRUCTURAL DETAILS
- 10 RISER REINF. STEEL DETAILS
- 14 CRADLE, ANTI-SEEP COLLARS AND STEEL DETAILS
- 12- POND DRAIN INLET DETAILS
- 13- IMPACT BASIN
- 44 TRASH RACKS, MID MISC DETAILS .
- 15 LOGS OF TEST HOLES
- 16 LOGS OF TEST HOLES

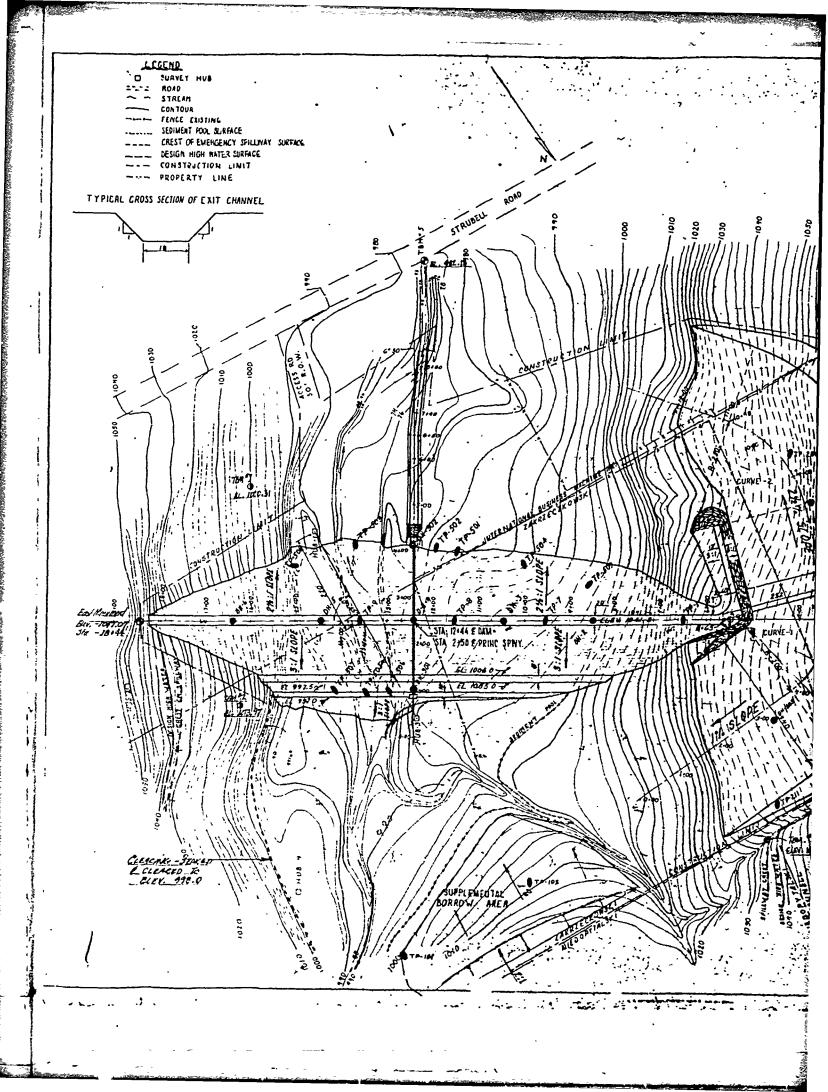


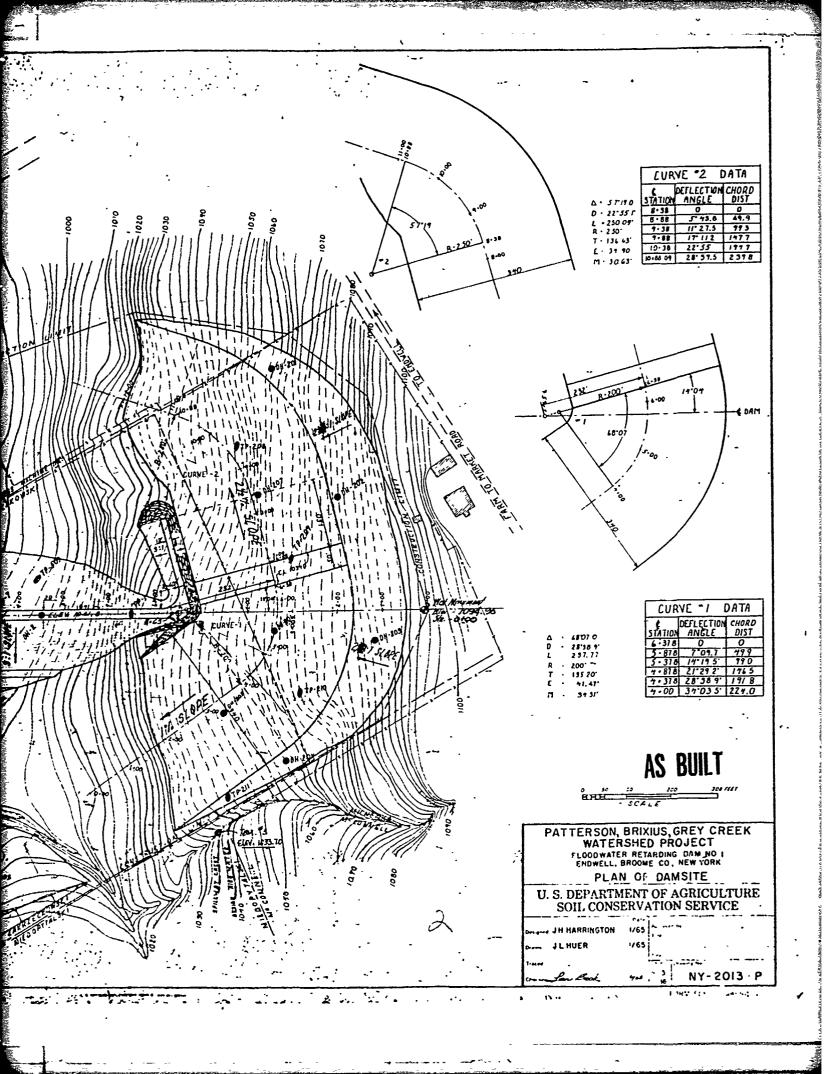
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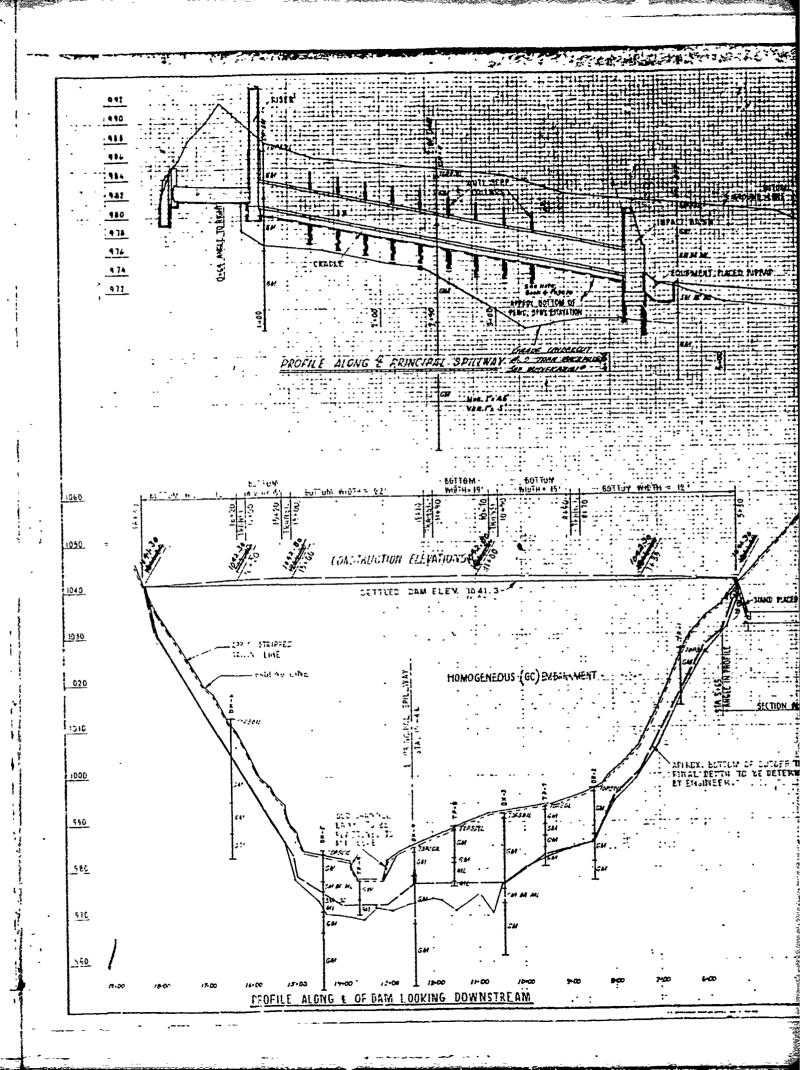
PATTERSON, BRIXIUS, GREY CREEK
WATERSHED PROJECT
FLOODWATER RETARDING DAM NO I
ENDWELL BROOME CO. NEW YORK
COVER SHEET

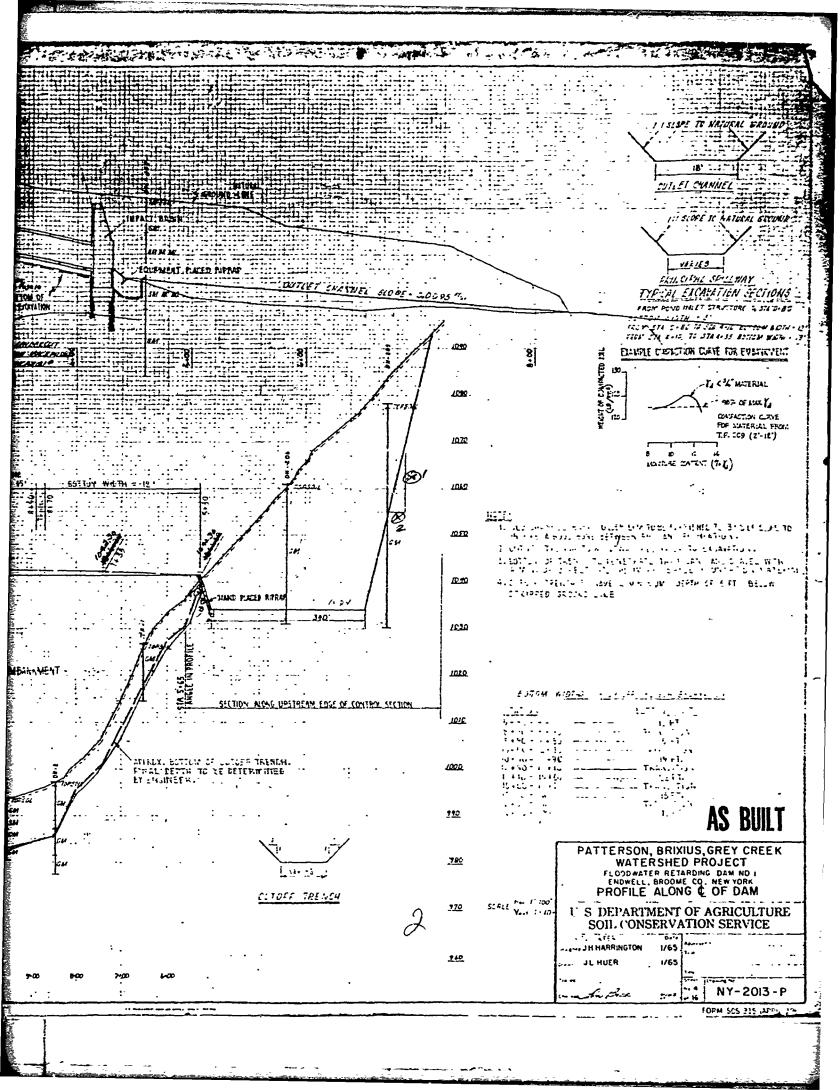
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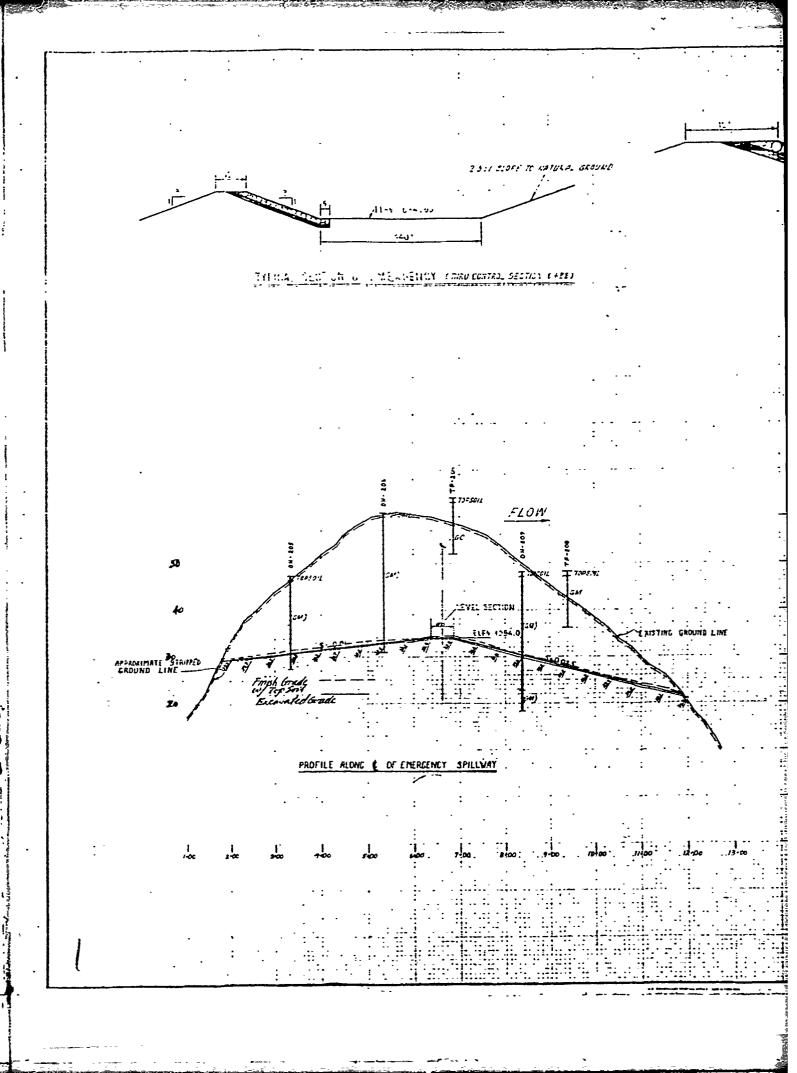
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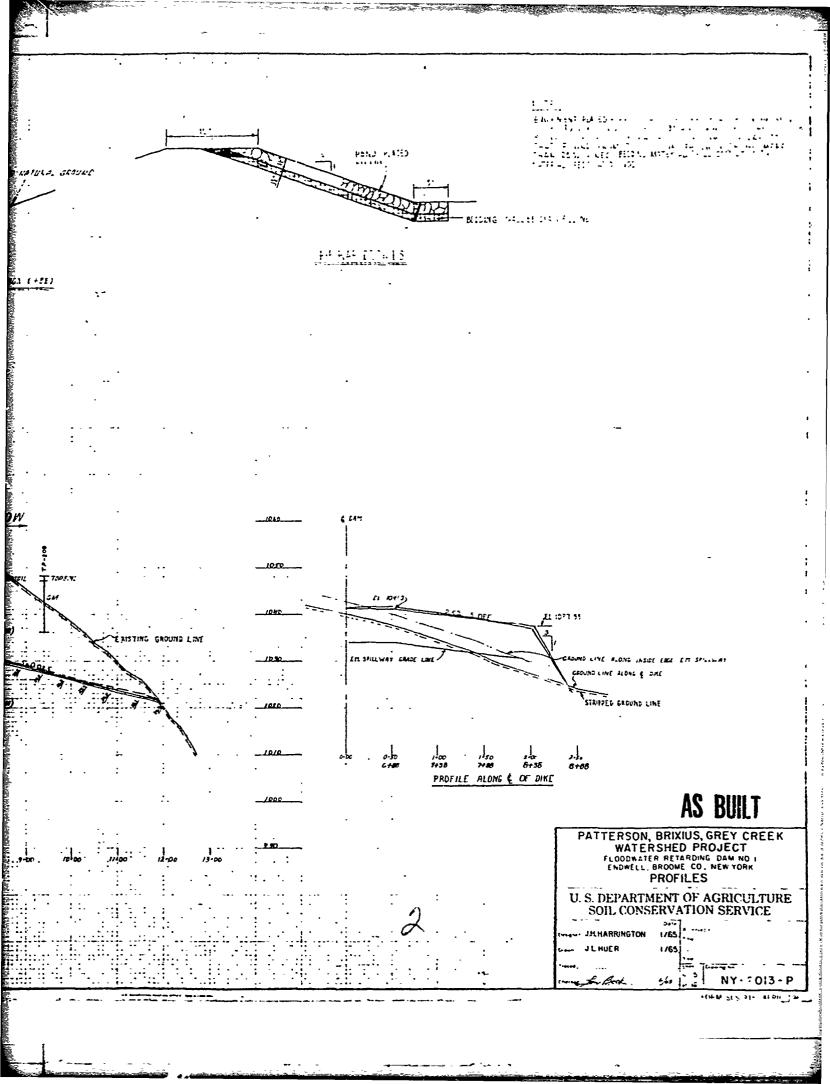




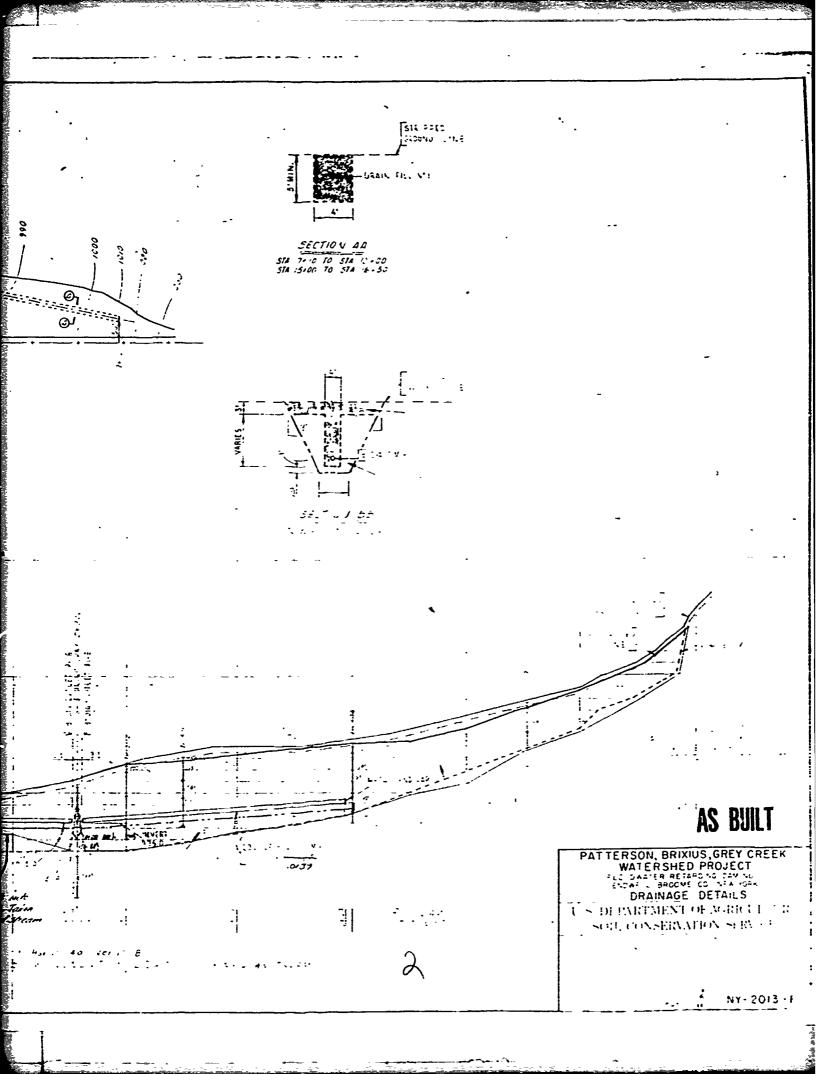


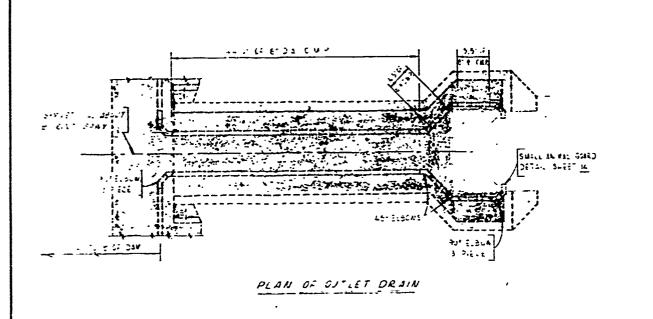


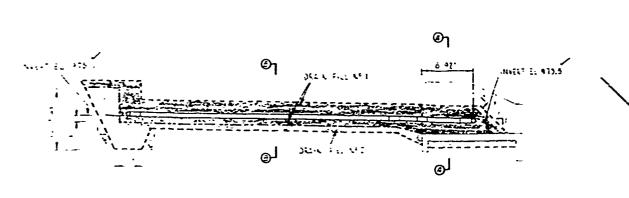




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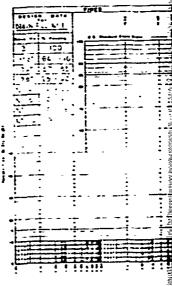


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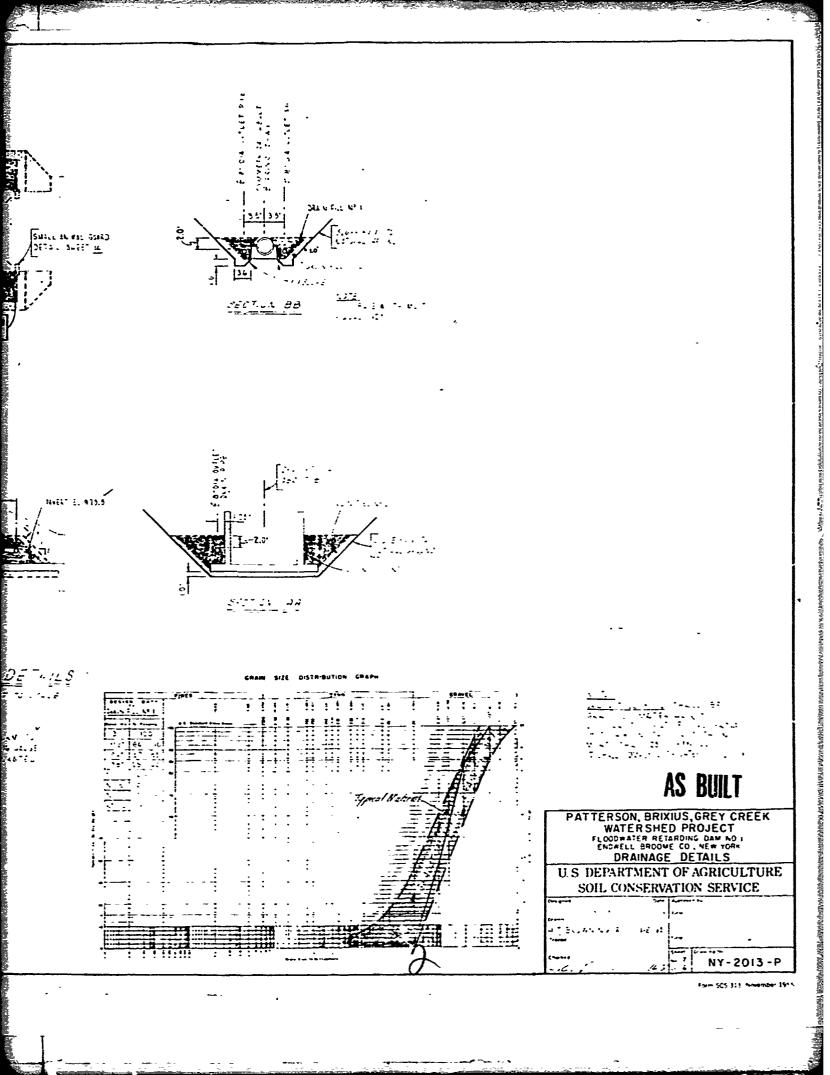
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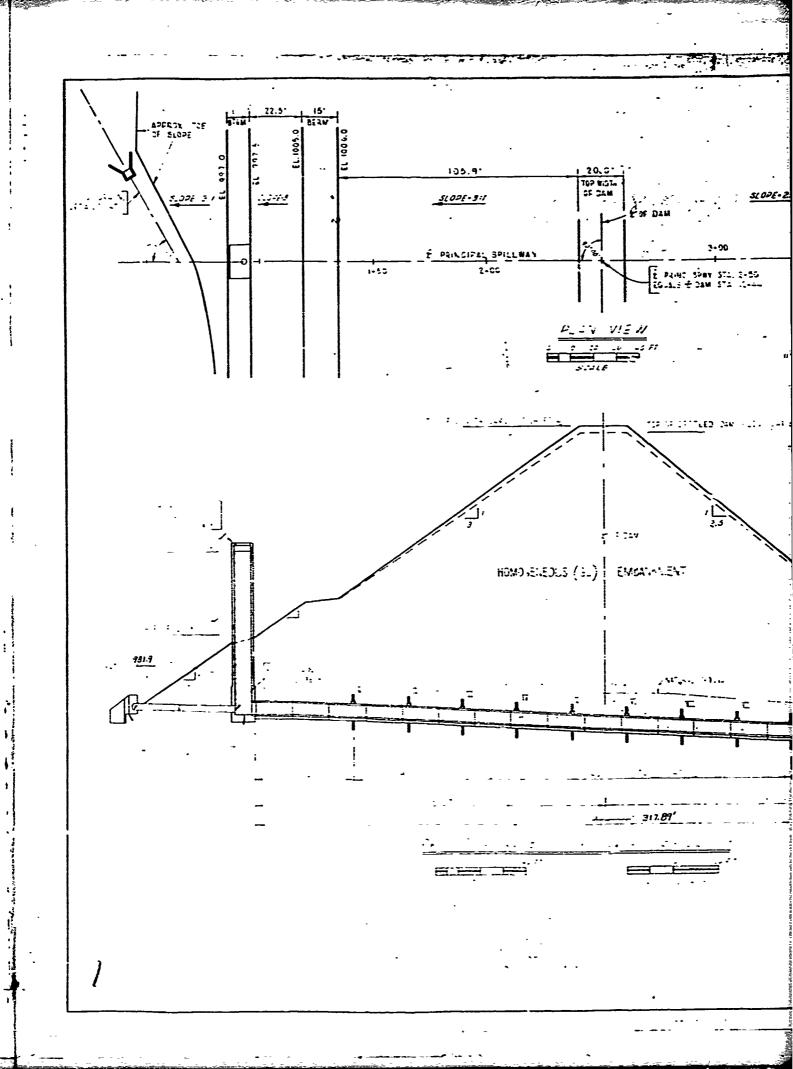
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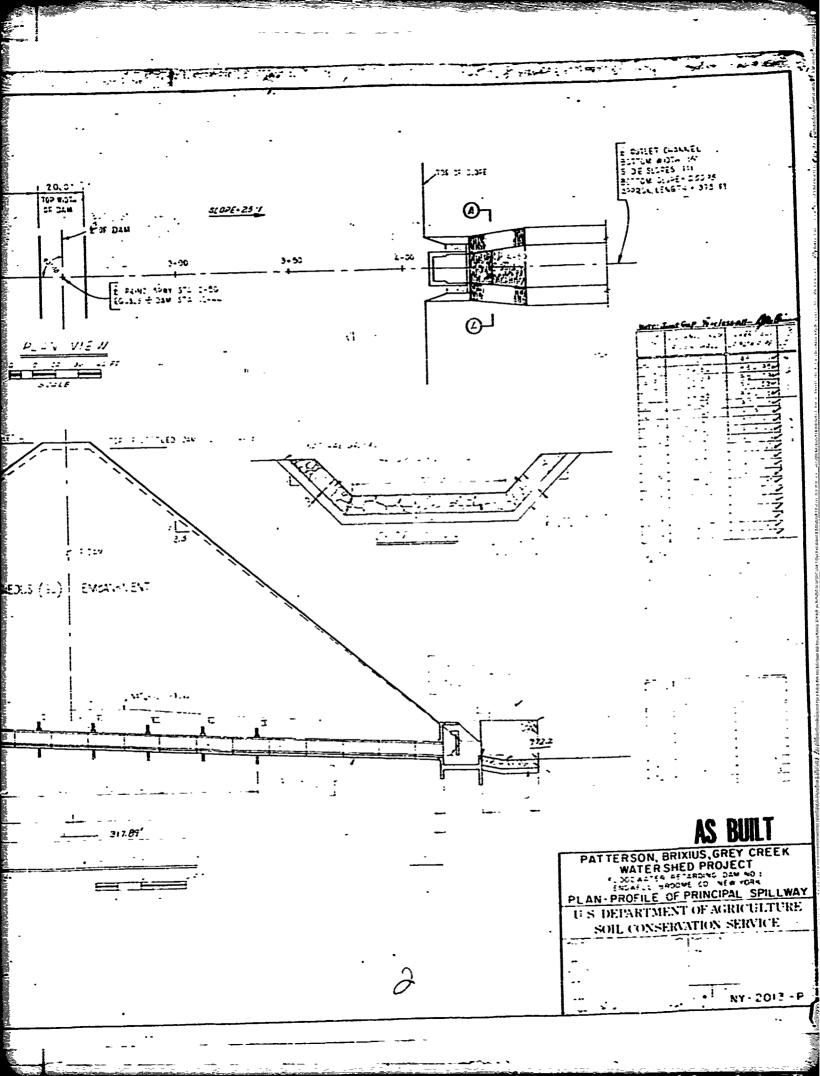


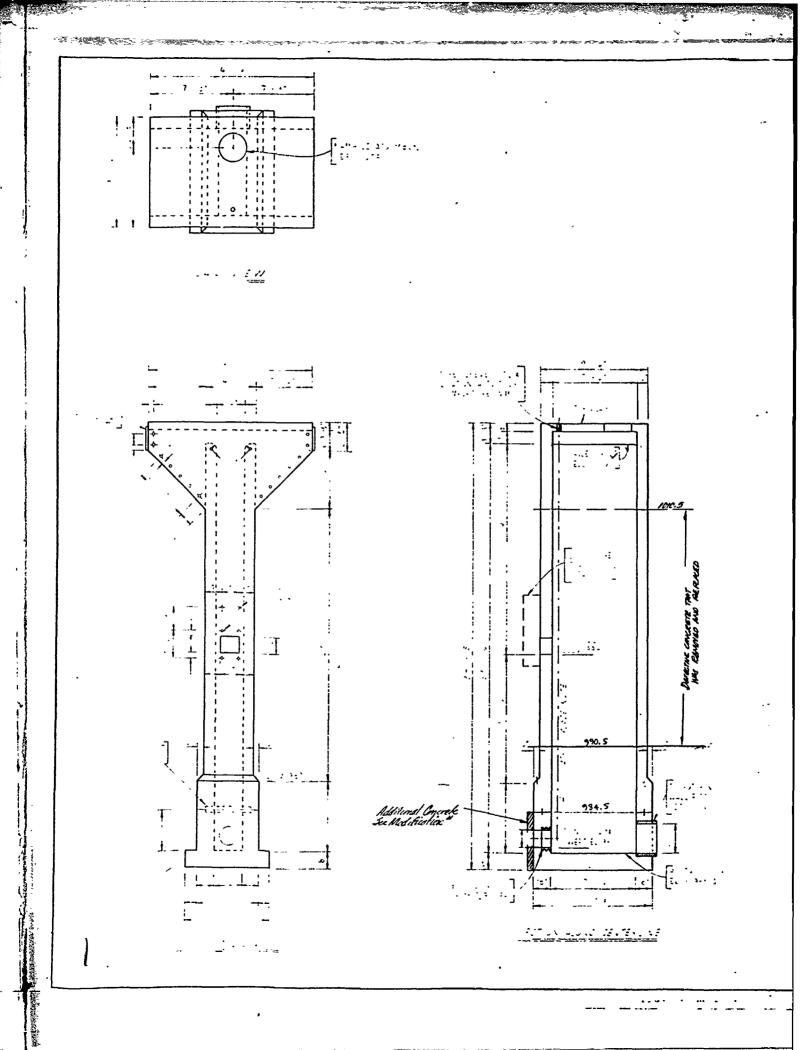
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SL'DE GATE NOTES

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E TAME ARE, THOMAS 9°CEST

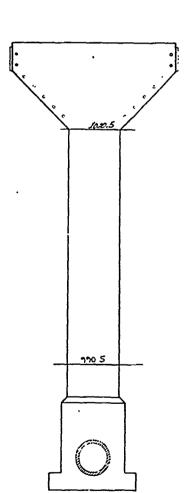
SUPPLIED : RODNEY HUNT MODEL 180

MANHOLE ASSEMBLY VOTE

I 30 DIA MANHOLE COVER WITH UNDERSIDE HOOKS AND A IT DIA MIN ROUND HOLE LIFTING DEVICE

2 PAINT IN ACCORDANCE WITH CONST SPEC 22

SUPPLIED: NEENAH FAUNDEY MODEL E-5900A



PLETE CONSTR. JOINT

AS BUILT

... ha e 642

PATTERSON, BRIXIUS, GREY CREEK
WATERSHED PROJECT
FLOODWATER RETARDING DAM NO I
ENDWELL BROOME CO, NEW YORK
RISER - STRUCTURAL DETAILS

U.S. DEPARTMENT OF AGRICULTURE

SOIL CONSERVATION SERVICE

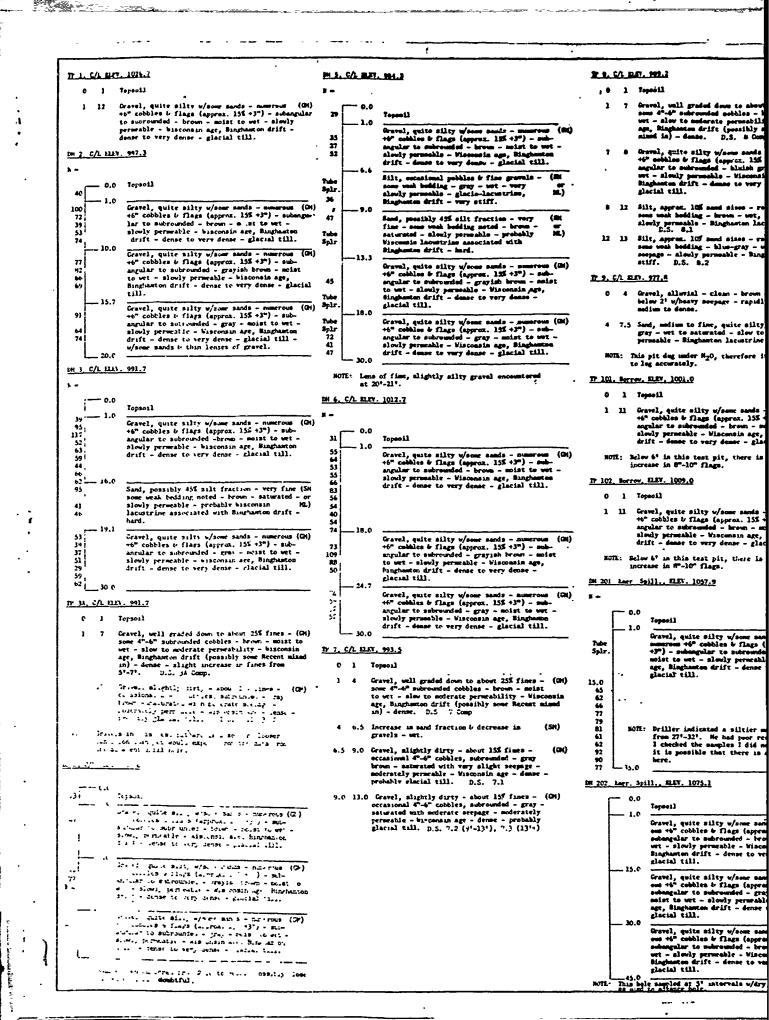
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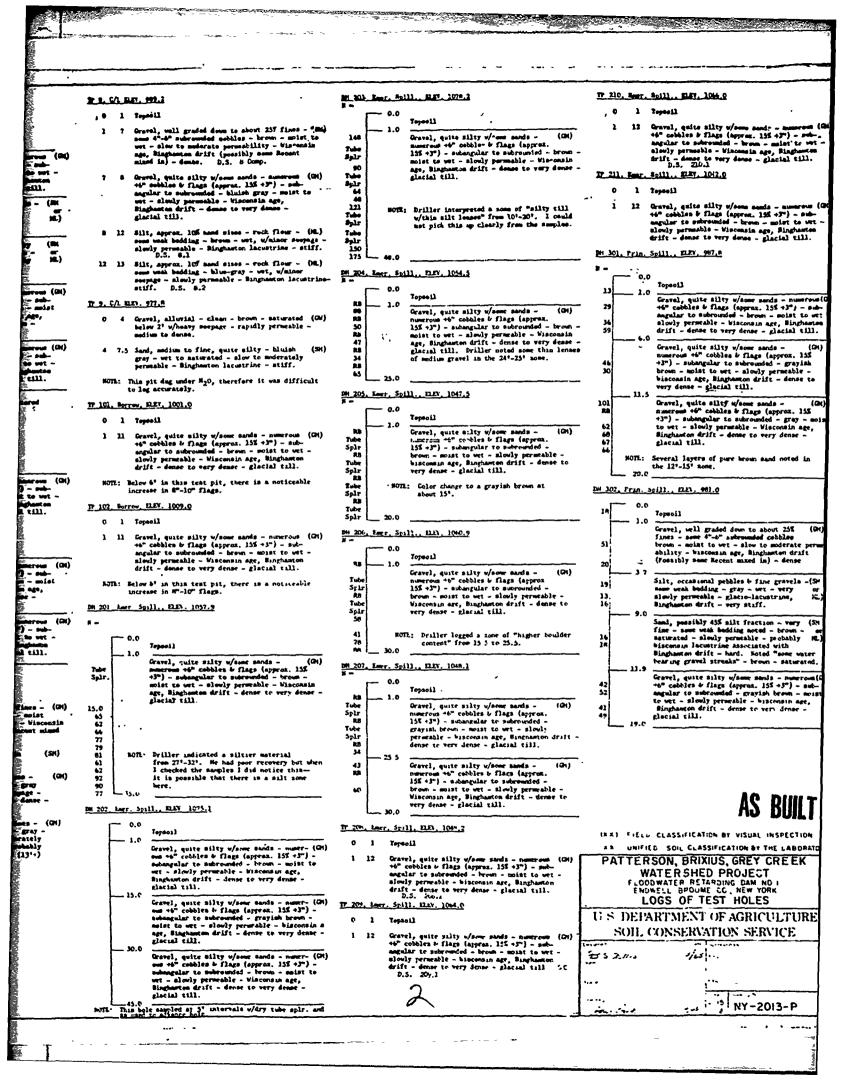
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990. S

984.5

X. 7.





11 501, 1 3, Top, 12.27 3mo, 1

1 Topsoil

Z No.

theoret, we'll graded down to about 257 (108) fines - over 47-67 subrausaled cobbles -house - moist to wet - slew to moderate permeability - biscensin see, Singhaston drift (possibly some Recent mixed in) -

- Gravel, quite silty w/some saids -numerous +6" cobbles : flags (apprex. 154 -3") subangular to subrounded -brown moist to wet slowly permeable -bisconsin age, Binefasten Jrift Jense to very dense clacial till.
- Silt, approx. 10% sand sizes rock flour- (ML) some weak bedding brown wet, w/manor se-page slowly permeable Ranghanton licustrane stiff.

Tr xv2, D S Tog, 11EV, 964.5

- Tousasi 1
- Gravel, well grated down to about 25% fines -(OH) some 4"-6" subrounded cobbles brown moist to wet slow to moderate perseability bisconsin are, hindbarton draft (possibly 5 some Recent wased n) - Jense.
- Silt, approx. 10% and sizes rock flour (ML) some weak bedding brown wet, w/minor seepage slowly permeable hingharton lacustrine stiff
- 9 12 5 bilt, approx. 105 sand sizes rock flour (ML) some weak bedding blue gray wet, w/minor seepage slouts perseable Binghamton lacustrime stiff.

Toe, HLEV. 976.0

- Gravel, alluvial clean brown saturated (Ob) below 2° with heavy seepage rapidly permeable -modium to dense Secent. 3
- Gravel, quite silty w/some sande numerous (Gt)
 +b" cobbles & flacs (approx 155 +3") subangular to subrounded blue frav moist to
 wet slowly permeable disconsin ace,
 Banghamton draft Jense to very dense glacial
- Will: Moderately dense from 3". of and year dense below of.

11 504, D 5. Tor ELEV. 587.0

- 1
- Gravel, well graded down to about 25% fines -(Ot) some 4"-6" subrounded robbles brown moist to wet slow to moderate permeability Wisconsin are, Blugharton drift (possibly some Recent mixed in) dense. D.S. >Ok Comp.
- Gravel, well graded down to about 25% fines -(CH) some 4"-6" subrounded cobbles brown saturated slow to mederate permeability Wisconsin are, Singhamton frift (possibly some Recent mixed in) dense.
- 10.5 Gravel, fine (pea gravel) considerable (Ga) sand grayish brown saturated moderate to rapidly permeable biscorsin age, Binghamton drift compact,
- 10 5 13.0 Sand, coarse w/some lenses of ondium to fine (SF)
 sand somewhat runny w/fairly heavy seepage brown mod. dense mid. perswable saturated.

Tee, BLFY, 941.5

- Gravel, alluvial clean brown saturated (OF) below 2° w/heavy scepare rapidly permeable -loose Recent. 3.5
- 3.5 13.0 Sant, and use to fine, quite silty bluish (SM) gray wet to saturated slow to inderately permeable Bing-artis, lacustrine stiff.

DP 50% .s. Tee, 124V. 579.3

- O 4 5 Gravel, alluvial clean heron saturated (Or) below 2" w/heavy became rapidly peneable -loose Recent.
- Sant, coarse, quite siity Suish grav wet (58) to sat. slow to maderately perceable Binguanton lacustrine stiff. 4.5 5.0

Tr 507, U.S. Toe 22.29, 955,2

0 3 5 Oravel, alluvial - clean - brown - saturated (Ov) below 2°- rapidly perm-able - 1 so - Recent.

- 3.5 5.5 Sand, medium to fine, quite milty brown (20) wet to mat. alow to maderately permeable Binghamton lacustrine stiff.
- 5.5 11.5 Sand, medium to fine, quite milty bluish gray(Bt) wet to sat. also to mederately permeable Binghamton lacustrine stiff.

Tr 50h, D.S Toe, ELEY, 983.0

- 0 1
- Cravel, quite silty w/some sands numerous (DN) +0" cobbles tr flags (approx. 155 +3") sub-angular to subrounded brown soist to set slowly permeable bisconsin age, Binghastco drift dense to very dense glacial till.
- Cravel, quite silty w/some sands numerous (OH) +6" cobbles to flage (approx. 155 *3") sub-angular to subrounded blue gray moist to set slowly permeable bisconsin age, bingharton drift dense to very dense glacial till.

IT 509 D.S. Toe 1118. 995.3

- Torsoil
- Cravel, quite silty w/some sands numerous (CM) +6" cobbles & flage (approx. 15% +3") sub-angular to subrounded brown some sottling to gray below 4" meist to set slewly permeable Visconsun age, Binghamton drift dense to very dense glacial till.
- Cravel, quite high in sands (sandy till) (OH-brown saturated (quite casy digging) -sod, permeable fairly heavy seepage at H* level (measured 7 g.p.m. flow into test pit) Binghauton drift (possibly an outwash remnant).

LUCCORD

Test Hole Numbering System

Centerline of dam	1 - 99
Borrey area	101 - 199
Emergency spillway	201 - 299
Centerline of outlet structure	301 - 399
Stream channel	401 - 499
Relief wells	501 - 599

UNIFIED SOIL CLASSIFICATION STSTEM STREETS

- OH Silty gravels; gravel-mand-milt mixtures ML Silts; milty, v.fine mands; mandy or elay
- Sand, silty travel, clean, well graded.

SAPLE

DS Disturbed

KEY TO DR'LL HOLE (DH) LOCS

¥ = 22]	N - Number of blovs required for 1 ft. standard penetration, using 2.0° 0.b. split barrel sampler, 140 lb. hammer, and 30° drop. ASTN D 1586.
	9.0 Bepth in bole (ft.) CL Unified Soil Classification Symbol 12.0
RS KI	Roller bit to advance hole by wash boring
KI 73%	Rock core, 2-1/8" diameter
50%	Percent rock core recovery in each drill rum
905	La Bedrock systel

- TEXT FIELD CLASSIFICATION BY VISUAL INSPECTION
- UNIFIED SOIL CLASSIFICATION BY THE LABORATORY

Marital

W

AS BUILT

PATTERSON, BRIXIUS, GREY CREEK
WATERSHED PROJECT
FLOCOMATER RETARDING DAM NO 1
ENDMEL BROOME CO. NEW YORK
LOGS OF TEST HOLES

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSTRUCTION SERVICE

SOIL CONSERVATION SERVICE

NY-2013- P